## Dual, 12-Bit, 40 MSPS MCM A/D Converter with Analog Input Signal Conditioning

## AD10242

## FEATURES

Two Matched ADCs with Input Signal Conditioning Selectable Bipolar Input Voltage Range
$( \pm 0.5 \mathrm{~V}, \pm 1.0 \mathrm{~V}, \pm 2.0 \mathrm{~V}$ )
Full MIL-STD-883B Compliant
80 dB Spurious-Free Dynamic Range
Trimmed Channel-Channel Matching
APPLICATIONS
Radar Processing
Communications Receivers
FLIR Processing
Secure Communications
Any I/Q Signal Processing Application

## PRODUCT DESCRIPTION

The AD 10242 is a complete dual signal chain solution including onboard amplifiers, references, ADCs, and output buffering providing unsurpassed total system performance. Each channel is laser trimmed for gain and offset matching and provides channel-to-channel crosstalk performance better than 80 dB . The AD 10242 utilizes two each of the AD 9631, OP279, and the AD 9042 in a custom M CM to gain space, performance, and cost advantages over solutions previously available.

The AD 10242 operates with $\pm 5.0 \mathrm{~V}$ for the analog signal conditioning with a separate +5.0 V supply for the analog-to-digital conversion. Each channel is completely independent allowing operation with independent encode or analog inputs. The AD 10242 also offers the user a choice of analog input signal ranges to minimize additional signal conditioning required for multiple functions within a single system. T he heart of the AD 10242 is the AD 9042 which is designed specifically for applications requiring wide dynamic range.
The AD 10242 is manufactured by Analog D evices on our M IL-PRF-38534 M CM line and is completely qualified. Units are packaged in a custom cofired ceramic 68-lead gull wing package and specified for operation from $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$. C ontact the factory for additional custom options including those which allow the user to ac couple the ADC directly, bypassing the front end amplifier section. Also see the AD 9042 data sheet for additional details on ADC performance.

## PRODUCT HIGHLIGHTS

1. Guaranteed sample rate of 40 M SPS .
2. Dynamic performance specified over entire $N$ yquist band; spurious signals @ 80 dBc for -1 dBF S input signals.
3. Low power dissipation: <2 W off $\pm 5.0 \mathrm{~V}$ supplies.
4. U ser defined input amplitude.
5. Packaged in 68 -lead ceramic leaded chip carrier.

FUNCTIONAL BLOCK DIAGRAM


REV. A

[^0][^1]
## AD10242- SPECIFICATIONS



|  | Temp | Test <br> Level | Mil <br> Subgroup | Min | AD 10242BZ/TZ <br> Typ | Max |
| :--- | :--- | :--- | :--- | :--- | :---: | :---: | Units


| Parameter | Temp | Test <br> Level | Mil Subgroup | AD 10242BZ/TZ |  |  | Units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Min | Typ | Max |  |
| SPURIOUS-FREE DYNAMIC RANGE ${ }^{9}$ <br> Analog Input <br> @ 1.2 M Hz <br> @ 4.85 M Hz <br> @ 9.9 M Hz <br> @ 19.5 M Hz | $\begin{aligned} & +25^{\circ} \mathrm{C} \\ & +25^{\circ} \mathrm{C} \\ & \text { Full } \\ & +25^{\circ} \mathrm{C} \\ & \text { Full } \\ & +25^{\circ} \mathrm{C} \\ & \text { Full } \end{aligned}$ | $\begin{aligned} & \text { I } \\ & \text { I } \\ & \text { II } \\ & \text { I } \\ & \text { II } \\ & \text { I } \end{aligned}$ | $\begin{aligned} & 4 \\ & 5,6 \\ & 4 \\ & 5,6 \\ & 4 \\ & 5,6 \end{aligned}$ | $\begin{aligned} & 70 \\ & 70 \\ & 63 \\ & 63 \\ & 60 \\ & 60 \end{aligned}$ | $\begin{aligned} & 81 \\ & 80 \\ & 79 \\ & 70 \\ & 69 \\ & 67 \\ & 66 \end{aligned}$ |  | dBFS <br> dBFS <br> dBFS <br> dBFS <br> dBFS <br> dBFS <br> dBFS |
| TWO-TONEIMD REJECTION ${ }^{10}$ F1, F2 @-7dBFS | Full | 11 | 4, 5, 6 | 70 | 76 |  | dBC |
| CHANNEL-TO-CHANNELISOLATION ${ }^{11}$ | $+25^{\circ} \mathrm{C}$ | IV | 12 | 75 | 80 |  | dB |
| TRANSIENT RESPONSE | $+25^{\circ} \mathrm{C}$ | V |  |  | 10 |  | ns |
| LINEARITY <br> Differential Nonlinearity (Encode $=20 \mathrm{MHz}$ ) Integral N onlinearity <br> (Encode $=20 \mathrm{M} \mathrm{Hz}$ ) | $\begin{aligned} & +25^{\circ} \mathrm{C} \\ & \text { Full } \\ & +25^{\circ} \mathrm{C} \\ & \text { Full } \end{aligned}$ | $\begin{aligned} & \text { IV } \\ & \text { IV } \\ & \text { V } \\ & \text { V } \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ |  | $\begin{aligned} & 0.3 \\ & 0.5 \\ & 0.3 \\ & 0.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.0 \\ & 1.25 \end{aligned}$ | $\begin{aligned} & \text { LSB } \\ & \text { LSB } \\ & \text { LSB } \\ & \text { LSB } \end{aligned}$ |
| OVERVOLTAGE RECOVERY TIME ${ }^{12}$ $\begin{aligned} & V_{I N}=2.0 \times F S \\ & V_{I N}=4.0 \times F S \end{aligned}$ | $\begin{aligned} & \text { Full } \\ & \text { Full } \end{aligned}$ | $\begin{aligned} & \text { IV } \\ & \text { IV } \end{aligned}$ | $\begin{aligned} & 12 \\ & 12 \end{aligned}$ |  | $\begin{aligned} & 50 \\ & 75 \end{aligned}$ | $\begin{aligned} & 100 \\ & 200 \end{aligned}$ | $\begin{aligned} & \text { ns } \\ & \text { ns } \end{aligned}$ |
| DIGITAL OUTPUTS Logic Compatibility Logic "1" Voltage ${ }^{13}$ Logic " 0 " Voltage ${ }^{14}$ Output C oding | Full Full | \| | $\begin{aligned} & 1,2,3 \\ & 1,2,3 \end{aligned}$ |  | $\begin{aligned} & \text { CM } \\ & 4.2 \\ & 0.45 \\ & \text { Compler } \end{aligned}$ | 0.65 | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ |
| POWER SUPPLY <br> AV ${ }_{\text {CC }}$ Supply Voltage I ( $\mathrm{V}_{\mathrm{CC}}$ ) Current AV $\mathrm{EE}^{\text {S }}$ Supply Voltage I ( $\mathrm{AV}_{\mathrm{EE}}$ ) Current DV ${ }_{\text {CC }}$ Supply Voltage I ( $D V_{C C}$ ) Current I CC (T otal) Supply Current Power Dissipation (T otal) Power Supply Rejection Ratio (PSRR) Pass Band Ripple to 10 M Hz | Full <br> Full <br> Full <br> Full <br> Full <br> Full <br> Full <br> Full <br> Full <br> Full | VI <br> V <br> VI <br> V <br> VI <br> V <br> I <br> I <br> I <br> IV | $\begin{aligned} & 1,2,3 \\ & 1,2,3 \\ & 7,8 \\ & 12 \end{aligned}$ |  | $\begin{aligned} & +5.0 \\ & 260 \\ & -5.0 \\ & 55 \\ & +5.0 \\ & 25 \\ & 350 \\ & 1.75 \\ & 0.01 \end{aligned}$ | $\begin{aligned} & 400 \\ & 2.0 \\ & 0.02 \\ & 0.2 \end{aligned}$ | V <br> mA <br> V <br> mA <br> V <br> mA <br> mA <br> W <br> \% FSR/\% V <br> dB |

## NOTES

${ }^{1}$ G ain tests are performed on $\mathrm{A}_{\text {IN }} 3$ over specified input voltage range.
${ }^{2}$ Input capacitance specifications combines AD 9631 die capacitance + ceramic package capacitance.
${ }^{3}$ Full power bandwidth is the frequency at which the spectral power of the fundamental frequency (as determined by FFT analysis) is reduced by 3 dB .

${ }^{5}$ ENCODE (Pin 4) may also be driven differentially in conjunction with ENCODE (Pin 5); see "Encoding the AD 10242" for details.
${ }^{6} \mathrm{M}$ inimum and maximum conversion rates allow for variation in Encode Duty Cycle of $50 \% \pm 5 \%$.
${ }^{7}$ Analog Input signal power at -1 dBFS; signal-to-noise ratio (SNR) is the ratio of signal level to total noise (first 5 harmonics removed). Encode $=40.0 \mathrm{M} \mathrm{SPS}$.
${ }^{8}$ Analog Input signal power at -1 dBFS ; signal-to-noise and distortion (SINAD) is the ratio of signal level to total noise + harmonics. Encode $=40.0 \mathrm{M} \mathrm{SPS}$.
${ }^{9}$ Analog Input signal equal -1 dBFS ; SFDR is ratio of converter full scale to worst spur.
${ }^{10}$ Both input tones at -7 dBFS ; two tone intermodulation distortion (IM D) rejection is the ratio of either tone to the worst 3rd order intermod product. f1 $=10.0 \mathrm{M} \mathrm{Hz}$ $\pm 100 \mathrm{kHz}, 50 \mathrm{kHz} \leq \mathrm{f} 1-\mathrm{f} 2 \leq 300 \mathrm{kHz}$.
${ }^{11}$ C hannel-to-channel isolation tested with A channel grounded and a full-scale signal applied to B channel (AIN 1).
${ }^{12}$ Input driven to $2 \times$ and $4 \times A_{\text {IN }} 1$ range for $>4$ clock cycles. Output recovers inband in specified time with E ncode $=40 \mathrm{MSPS}$. No foldover guaranteed.
${ }^{13}$ Outputs are sourcing $10 \mu \mathrm{~A}$.
${ }^{14} 0$ utputs are sinking $10 \mu \mathrm{~A}$.
All specifications guaranteed within 100 ms of initial power up regardless of sequencing.
Specifications subject to change without notice.

## ABSOLUTE MAXIMUM RATINGS ${ }^{1}$

| Parameter | Min | Max | Units |
| :--- | :--- | :--- | :--- |
| ELECTRICAL |  |  |  |
| V CC Voltage $^{V_{\text {EE }} \text { Voltage }}$ | 0 | 7 | V |
| Analog Input V oltage | -7 | 0 | V |
| Analog Input Current | $\mathrm{V}_{\mathrm{EE}}$ | $\mathrm{V}_{\mathrm{CC}}$ | V |
| Digital Input Voltage (EN CODE) | -10 | +10 | mA |
| ENCODE, ENCODE D ifferential Voltage | 0 | $\mathrm{~V}_{\mathrm{CC}}$ | V |
| Digital Output Current | -40 | 4 | V |
| EN VIRON M EN TAL ${ }^{2}$ |  |  | mA |
| $\quad$ Operating T emperature (C ase) | -55 | +125 | ${ }^{\circ} \mathrm{C}$ |
| M aximum Junction T emperature |  | +175 | ${ }^{\circ} \mathrm{C}$ |
| Lead Temperature (Soldering, 10 sec) |  | +300 | ${ }^{\circ} \mathrm{C}$ |
| Storage T emperature Range (Ambient) | -65 | +150 | ${ }^{\circ} \mathrm{C}$ |

NOTES
${ }^{1}$ Absolute maximum ratings are limiting values to be applied individually, and beyond which the serviceability of the circuit may be impaired. Functional operability is not necessarily implied. Exposure to absolute maximum rating conditions for an extended period of time may affect device reliability.
${ }^{2}$ Typical thermal impedances for "Z" package: $\theta_{\mathrm{J}}=11^{\circ} \mathrm{C} / \mathrm{W} ; \theta_{\mathrm{JA}}=30^{\circ} \mathrm{C} / \mathrm{W}$.

Table I. Output Coding

| MSB LSB | Base 10 | Input |
| :--- | :--- | :--- |
| 0111111111111 | 2047 | +FS |
| 0000000000001 | +1 |  |
| 0000000000000 | 0 | 0.0 V |
| 1111111111111 | -1 | -FS |
| 1000000000000 | 2048 |  |

## EXPLANATION OF TEST LEVELS

## Test Level

I - 100\% Production T ested.
II - $100 \%$ production tested at $+25^{\circ} \mathrm{C}$, and sample tested at specified temperatures. AC testing done on sample basis.
III - Sample Tested Only.
IV - Parameter is guaranteed by design and characterization testing.
V - Parameter is a typical value only.
VI - All devices are $100 \%$ production tested at $+25^{\circ} \mathrm{C}$; sample tested at temperature extremes.

## ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| AD 10242BZ | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ (C ase) | 68-Pin C eramic L eaded C hip C arrier | Z-68A |
| AD 10242T Z | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ (C ase) | 68-Pin C eramic L eaded C hip C arrier | Z-68A |
| AD 10242T Z/883B | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ (C ase) | 68 -Pin Ceramic L eaded C hip C arrier | Z-68A |
| $5962-9581501 \mathrm{HXA}$ | $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$ (C ase) | 68 -Pin Ceramic Leaded C hip C arrier | Z-68A |
| AD 10242/PC B | $+25^{\circ} \mathrm{C}$ | Evaluation Board with AD 10242BZ |  |

## CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD 10242 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

PIN FUNCTION DESCRIPTIONS

| Pin No. | Name | Function |
| :---: | :---: | :---: |
| 1 | SHIELD | Internal Ground Shield between channels. |
| 2, 5, 9-11, 26-27 | GNDA | A Channel G round. A and B grounds should be connected as close to the device as possible. |
| 3 | UNEGA | U nipolar N egative. |
| 4 | UCOMA | U nipolar Common. |
| 6 | $\mathrm{A}_{\text {IN }} \mathrm{Al} 1$ | Analog Input for A side ADC ( ( |
| 7 | $\mathrm{A}_{\text {IN }} \mathrm{A} 2$ | Analog Input for A side ADC ( $n o m i n a l l y ~ \pm 1.0 \mathrm{~V}$ ). |
| 8 | $A_{\text {IN }} \mathrm{A} 3$ | Analog Input for A side ADC ( $n o m i n a l l y ~ \pm 2.0 \mathrm{~V}$ ). |
| 12 | UPOSA | U nipolar Positive. |
| 13 | $\mathrm{AV}_{\mathrm{EE}}$ | Analog N egative Supply Voltage ( $n o m i n a l l y-5.0 \mathrm{~V}$ or -5.2 V ). |
| 14 | $A V_{\text {cc }}$ | Analog Positive Supply Voltage (nominally +5.0 V ). |
| 15-16 | NC | No Connect. |
| 17-25, 31-33 | D0A-D 11A | Digital Outputs for ADC A. D 0 (LSB). |
| 28 | ENCODEA | $\overline{\text { ENCODE }}$ is complement of ENCODE. |
| 29 | ENCODEA | D ata conversion initiated on rising edge of ENCODE input. |
| 30 | $D V_{C C}$ | Digital positive supply voltage (nominally +5.0 V ). |
| 34-35 | NC | N o Connect. |
| 36-42, 45-49 | D 0B-D 11B | Digital O utputs for ADC B. D 0 (LSB). |
| 43-44, 53-54 | GNDB | $B C$ hannel Ground. $A$ and $B$ grounds should be connected as close to the device |
| 58-61, 65, 68 |  | as possible. |
| 50 | DV ${ }_{\text {CC }}$ | D igital Positive Supply Voltage (nominally +5.0 V). |
| 51 | ENCODEB | D ata conversion initiated on rising edge of ENCODE input. |
| 52 | $\overline{\text { ENCODEB }}$ | $\overline{\text { ENCODE }}$ is complement of ENCODE. |
| 55 | UCOMB | U nipolar Common. |
| 56 | UNEGB | U nipolar N egative. |
| 57 | UPOSB | U nipolar Positive. |
| 62 | $\mathrm{A}_{\text {IN }} \mathrm{B} 1$ |  |
| 63 | $\mathrm{A}_{\text {IN }} \mathrm{B} 2$ | Analog Input for B side ADC ( $n$ minally $\pm 1.0 \mathrm{~V}$ ). |
| 64 | $\mathrm{A}_{\text {IN }} \mathrm{B} 3$ | Analog Input for B side ADC (nominally $\pm 2.0 \mathrm{~V}$ ). |
| 66 | $A V_{\text {cc }}$ | Analog Positive Supply Voltage (nominally +5.0 V ). |
| 67 | $\mathrm{AV}_{\mathrm{EE}}$ | Analog N egative Supply V oltage (nominally -5.0 V or -5.2 V ). |

PIN CONFIGURATION
68-Lead Ceramic Leaded Chip Carrier


## AD10242

## DEFINITION OF SPECIFICATIONS

## Analog Bandwidth

The analog input frequency at which the spectral power of the fundamental frequency (as determined by the FFT analysis) is reduced by 3 dB .

## Aperture Delay

The delay between the $50 \%$ point of the rising edge of the ENCODE command and the instant at which the analog input is sampled.

## Aperture Uncertainty (Jitter)

T he sample-to-sample variation in aperture delay.

## Differential Nonlinearity

The deviation of any code from an ideal 1 LSB step.

## Encode Pulse Width/Duty Cycle

Pulse width high is the minimum amount of time that the ENCODE pulse should be left in logic " 1 " state to achieve rated performance; pulse width low is the minimum time ENCODE pulse should be left in low state. At a given clock rate, these specs define an acceptable Encode duty cycle.

## Harmonic Distortion

The ratio of the rms signal amplitude to the rms value of the worst harmonic component.

## Integral Nonlinearity

The deviation of the transfer function from a reference line measured in fractions of 1 LSB using a "best straight line" determined by a least square curve fit.

## Minimum Conversion Rate

The encode rate at which the SN R of the lowest analog signal frequency drops by no more than 3 dB below the guaranteed limit.

## Maximum Conversion Rate

T he encode rate at which parametric testing is performed.

## Output Propagation Delay

The delay between the $50 \%$ point of the rising edge of ENCODE command and the time when all output data bits are within valid logic levels.

## Overvoltage Recovery Time

The amount of time required for the converter to recover to $0.02 \%$ accuracy after an analog input signal of the specified percentage of full scale is reduced to midscale.

## Power Supply Rejection Ratio

The ratio of a change in input offset voltage to a change in power supply voltage.

## Signal-to-Noise-and-Distortion (SINAD)

The ratio of the rms signal amplitude (set at 1 dB below full scale) to the rms value of the sum of all other spectral components, including harmonics but excluding dc .

## Signal-to-Noise Ratio (without Harmonics)

The ratio of the rms signal amplitude (set at 1 dB below full scale) to the rms value of the sum of all other spectral components, excluding the first five harmonics and dc.

## Spurious-Free Dynamic Range

The ratio of the rms signal amplitude to the rms value of the peak spurious spectral component. The peak spurious component may or may not be a harmonic. M ay be reported in dBc (i.e., degrades as signal levels is lowered) or in dBFS (always related back to converter full scale).

## Transient Response

The time required for the converter to achieve $0.02 \%$ accuracy when a one-half full-scale step function is applied to the analog input.

## Two-Tone Intermodulation Distortion Rejection

The ratio of the rms value of either input tone to the rms value of the worst third order intermodulation product; reported in dBc.

## Two-Tone SFDR

The ratio of the rms value of either input tone to the rms value of the peak spurious component. The peak spurious component may or may not be an IM D product. M ay be reported in dBc (i.e., degrades as signal levels is lowered) or in dBFS (always related back to converter full scale).


Figure 1. Timing Diagram


Figure 2. Equivalent Burn-In Circuit

## EQUIVALENT CIRCUITS



Figure 3. Analog Input Stage


Figure 4. Encode Inputs


Figure 6. Single Tone @ 4.85 MHz


Figure 7. Single Tone @ 9.9 MHz


Figure 8. Single Tone @ 19.5 MHz


Figure 9. Two Tone FFT @ 9.8/10.1 M Hz


Figure 10. Two Tone FFT @ 19.5/19.7 MHz


Figure 11. Harmonics vs. AIN


Figure 12. SNR vs. $A_{i N}$


Figure 13. SNR and Harmonics vs. Encode Rate


Figure 14. Offset and Gain Error vs. Temperature


Figure 15. Isolation vs. Frequency


Figure 16. Single Tone SFDR ( $A_{I N} @ 9.98$ ) vs. Power Level


Figure 17. Single Tone SFDR ( $A_{I N} @ 19.9$ ) vs. Power Level

## AD10242- Typical Performance Characteristics



Figure 18. SNR/Harmonics to $A_{I N}>$ Nyquist MSPS


Figure 19. Gain Flatness vs. Input Frequency

## THEORY OF OPERATION

Refer to the block diagram. The AD 10242 employs three monolithic ADI components per channel (AD 9631, OP279, and AD 9042), along with multiple passive resistor networks and decoupling capacitors to fully integrate a complete 12-bit analog-to-digital converter.
The input signal is first passed through a precision laser trimmed resistor divider allowing the user to externally select operation with a full scale signal of $\pm 0.5 \mathrm{~V}, \pm 1.0 \mathrm{~V}$, or $\pm 2.0 \mathrm{~V}$ by choosing the proper input terminal for the application. The result of the resistor divider is to apply a full-scale input of approximately 0.4 V to the noninverting input of the internal AD 9631 amplifier.
The AD 9631 provides the dc coupled level shift circuit required for operation with the AD 9042 ADC. C onfiguring the amplifier in a noninverting mode the ac signal gain can be trimmed to provide a constant input to the ADC centered around the internal reference voltage of the AD 9042. This allows the converter to be used in multiple system applications without the need for external gain and level shift circuitry normally requiring trim. The AD 9631 was chosen for its superior ac performance and input drive capabilities which have limited the ability of many amplifiers to drive high performance ADCs. As new amplifiers are developed, pin compatible improvements are planned to incorporate the latest operational amplifier technology.
The OP279 provides the buffer and inversion of the internal reference of the AD 9042 in order to supply the summing node of the AD 9631 input amplifier. This dc voltage is then summed with the input voltage and applied to the input of the AD 9042 ADC. The reference voltage of the AD 9042 is designed to track internal offsets and drifts of the ADC and is used to ensure matching over an extended temperature range of operation.

## APPLYING THE AD10242 <br> Encoding the AD 10242

The AD 10242 is designed to interface with TTL and CM OS logic families. The source used to drive the EN CODE pin(s) must be clean and free from jitter. Sources with excessive jitter will limit SNR and overall performance.


Figure 20. Single-Ended TTL/CMOS Encode
The AD 10242 encode inputs are connected to a differential input stage (see Figure 4 under EQUIVALENT CIRCUITS). With no input connected to either the ENCODE or input, the voltage divider bias the inputs to 1.6 volts. F or TTL or CM OS usage, the encode source should be connected to EN CODE (Pins 29 and/or 51). $\overline{\text { ENCODE }}$ (Pins 28 and/or 52) should be decoupled using a low inductance or microwave chip capacitor to ground. Devices such as AVX 05085C 103M A15, a $0.01 \mu \mathrm{~F}$ capacitor, work well.

## Performance Improvements

It is possible to improve the performance of the AD 10242 slightly by taking advantage of the internal characteristics of the amplifier and converter combination. By increasing the +5 V supply slightly, the user may be able to gain up to a 5 dB improvement in SF D R over the entire frequency range of the converter. It is not recommended to exceed +5.5 V on the analog supplies as there are no performance benefits beyond that range and care should be taken to avoid the absolute maximum ratings.

If a logic threshold other than the nominal 1.6 V is required, the following equations show how to use an external resistor, $R_{x}$, to raise or lower the trip point (see Figure $4, R 1=17 \mathrm{k} \Omega$, $R 2=8 \mathrm{k} \Omega$ ).
$V_{1}=\frac{5 R 2 R_{x}}{R 1 R 2+R 1 R_{x}+R 2 R_{x}}$ to lower logic threshold.


Figure 21. Lower Threshold for Encode
$V_{1}=\frac{5 R 2}{R 2+\frac{R 1 R_{x}}{R 1+R_{x}}}$ to raise logic threshold.


Figure 22. Raise Logic Threshold for Encode
While the single ended encode will work well for many applications, driving the encode differentially will provide increased performance. Depending on circuit layout and system noise, a 1 dB to 3 dB improvement in SNR can be realized. It is recommended that the encode signal be ac-coupled into the EN CODE and ENCODE pins.
The simplest option is shown below. The low jitter T TL signal is coupled with a limiting resistor, typically $100 \Omega$, to the primary side of an RF transformer (these transformers are inexpensive and readily available; Part No . in figure is from M iniCircuits). The secondary side is connected to the ENCODE and ENCODE pins of the converter. Since both encode inputs are self-biased, no additional components are required.


Figure 23. TTL Source—Differential Encode

If no T TL source is available, a clean sine wave may be substituted. In the case of the sine source, the matching network is shown below. Since the matching transformer specified is a 1:1 impedance ratio, $R$, the load resistor should be selected to match the source impedance. The input impedance of the AD 9042 is negligible in most cases.


Figure 24. Sine Source—Differential Encode If a low jitter ECL clock is available, another option is to accouple a differential ECL signal to the encode input pins as shown below. The capacitors shown here should be chip capacitors but do not need to be of the low inductance variety.


Figure 25. Differential ECL for Encode
As a final alternative, the ECL gate may be replaced by an ECL comparator. The input to the comparator could then be a logic signal or a sine signal.


Figure 26. ECL Comparator for Encode
C are should be taken not to overdrive the encode input pin when ac coupled. Although the input circuitry is electrically protected from over or under voltage conditions, improper circuit operations may result from overdriving the encode input pin.

## AD10242

## USING THE FLEXIBLE INPUT

The AD 10242 has been designed with the user's ease of operation in mind. M ultiple input configurations have been included on board to allow the user to have a choice of input signal levels and input impedance. While the standard inputs are $\pm 0.5 \mathrm{~V}$, $\pm 1.0 \mathrm{~V}$, and $\pm 2.0 \mathrm{~V}$, the user can select the input impedance of the AD 10242 on any input by using the other inputs as alternate locations for GND or an external resistor. The following chart summarizes the impedance options available at each input location:
$A_{I N} 1=100 \Omega$ when $A_{I N} 2$ and $A_{I N} 3$ Are 0 pen.
$A_{\text {IN }} 1=75 \Omega$ when $A_{I N} 3$ Is Shorted to GND.
$A_{\text {IN }} 1=50 \Omega$ when $A_{\text {IN }} 2$ Is Shorted to GND.
$\mathrm{A}_{\text {IN }} 2=200 \Omega$ when $\mathrm{A}_{\text {IN }} 3$ Is 0 pen.
$A_{\text {IN }} 2=100 \Omega$ when $A_{\text {IN }} 3$ Is Shorted to GND.
$\mathrm{A}_{\text {IN }} 2=75 \Omega$ when $\mathrm{A}_{\text {IN }} 2$ to $\mathrm{A}_{\text {IN }} 3 \mathrm{H}$ as an External R esistor of $300 \Omega$, with $A_{\text {IN }} 3$ Shorted to GND.
$\mathrm{A}_{\text {IN }} 2=50 \Omega$ when $\mathrm{A}_{\text {IN }} 2$ to $\mathrm{A}_{\text {IN }} 3 \mathrm{H}$ as an External R esistor of $100 \Omega$, with $\mathrm{A}_{\text {IN }} 3$ Shorted to GND.
$A_{\text {IN }} 3=400 \Omega$.
$\mathrm{A}_{\text {IN }} 3=100 \Omega$ when $\mathrm{A}_{\text {IN }} 3 \mathrm{H}$ as an External Resistor of $133 \Omega$ to GND. $A_{\text {IN }} 3=75 \Omega$ when $A_{\text {IN }} 3 \mathrm{H}$ as an External Resistor of $92 \Omega$ to GND. $A_{\text {IN }} 3=50 \Omega$ when $A_{\text {IN }} 3 \mathrm{H}$ as an External Resistor of $57 \Omega$ to GND.
While the A nalog inputs of the AD 10242 are designed for dc coupled bipolar inputs, the AD 10242 has the ability to use unipolar inputs in a user selectable mode through the addition of a external resistor. This allows for $1 \mathrm{~V}, 2 \mathrm{~V}$, and 4 V full-scale unipolar signals to be applied to the various inputs ( $\mathrm{A}_{I N} 1, \mathrm{~A}_{I N} 2$, and $A_{\text {IN }} 3$ respectively). Placing a $2.43 \mathrm{k} \Omega$ resistor (typical, offset calibration required) between UPOS and UCOM shifts the reference voltage setpoint to allow a unipolar positive voltage to be applied at the inputs of the device. To calibrate offset a midscale dc voltage should be applied to the converter while adjusting the unipolar resistor for a midscale output transition.


Figure 27. Unipolar Positive
To operate with $-1 \mathrm{~V},-2 \mathrm{~V}$, or -4 V full-scale unipolar signals place a $2.67 \mathrm{k} \Omega$ resistor (typical, offset calibration required) between UN EG and UCOM. This again shifts the reference voltage setpoint to allow a unipolar negative voltage to be applied at the inputs of the device. T o calibrate offset a midscale dc voltage should be applied to the converter while adjusting the unipolar resistor for a midscale output transition.


Figure 28. Unipolar Negative

## GROUNDING AND DECOUPLING

## Analog and Digital Grounding

Proper grounding is essential in any high speed, high resolution system. M ultilayer printed circuit boards (PCBs) are recommended to provide optimal grounding and power schemes. The use of ground and power planes offers distinct advantages:

1. The minimization of the loop area encompassed by a signal and its return path.
2. The minimization of the impedance associated with ground and power paths.
3. The inherent distributed capacitor formed by the power plane, PCB insulation, and ground plane.
These characteristics result in both a reduction of electromagnetic interference (EMI) and an overall improvement in performance.
It is important to design a layout that prevents noise from coupling to the input signal. Digital signals should not be run in parallel with input signal traces and should be routed away from the input circuitry. The AD 10242 does not distinguish between analog and digital ground pins as the AD 10242 should always be treated like an analog component. All ground pins should be connected together directly under the AD 10242. The PCB should have a ground plane covering all unused portions of the component side of the board to provide a low impedance path and manage the power and ground currents. The ground plane should be removed from the area near the input pins to reduce stray capacitance.

## LAYOUT INFORMATION

The schematic of the evaluation board (Figure 29) represents a typical implementation of the AD 10242. The pinout of the AD 10242 is very straightforward and facilitates ease of use and the implementation of high frequency/high resolution design practices. It is recommended that high quality ceramic chip capacitors be used to decouple each supply pin to ground directly at the device. All capacitors except the one placed on $\overline{\text { ENCODE }}$ can be standard high quality ceramic chip capacitors. The capacitor used on ENCODE pin must be a low inductance chip capacitor as referenced previously in the data sheet.


Figure 29. Evaluation Board Schematic

## AD10242

Care should be taken when placing the digital output runs. Because the digital outputs have such a high slew rate, the capacitive loading on the digital outputs should be minimized. C ircuit traces for the digital outputs should be kept short and connect directly to the receiving gate. Internal circuitry buffers the outputs of the AD 9042 ADC through a resistor network to eliminate the need to externally isolate the device from the receiving gate.

EVALUATION BOARD
The AD 10242 evaluation board (see Figure 30) is designed to provide optimal performance for evaluation of the AD 10242
analog-to-digital converter. The board encompasses everything needed to ensure the highest level of performance for evaluating the AD 10242.
Power to the analog supply pins is connected via banana jacks. The analog supply powers the crystal oscillator, the associated components and amplifiers, and the analog section of the
AD 10242. The D igital outputs of the AD 10242 are powered via Pin 1 of either J9 or J10 found on the digital interface connector. To power the evaluation board with one +5 V supply a jumper wire is required from test point E1 to E4. Contact the factory if additional layout or applications assistance is required.


Figure 30. Evaluation Board Mechanical Layout

## OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).



[^0]:    Information furnished by Analog Devices is believed to be accurate and reliable. However, no responsibility is assumed by Analog Devices for its use, nor for any infringements of patents or other rights of third parties which may result from its use. No license is granted by implication or otherwise under any patent or patent rights of Analog Devices.

[^1]:    One Technology Way, P.O. Box 9106, Norwood, MA 02062-9106, U.S.A.
    Tel: 617/329-4700 World Wide Web Site: http://www.analog.com Fax: 617/326-8703 © Analog Devices, Inc., 1997

