

## 2W Stereo Audio Amplifier with No Headphone Coupling Capacitor Function

### Features

- Depop Circuitry Integrated
- Output Power at 1% THD+N, VDD=5V
  - 1.8W/CH (typical) into a 4Ω Load
  - 1.2W/CH (typical) into a 8Ω Load
- Eliminates Headphone Amplifier Output Coupling Capacitors
- Maximum Output Power Clamping Circuitry Integrated
- Bridge-Tied Load (BTL), Single-Ended (SE), and Stereo Headphone Amplifier (HP-IN) modes Supported
- Stereo Input MUX
- Mute and Shutdown Control Available
- Surface-Mount Power Package  
24-Pin TSSOP-P

### Applications

- Stereo Power Amplifiers for Notebooks or Desktop Computers
- Multimedia Monitors
- Stereo Power Amplifiers for Portable Audio Systems

### General Description

G1421 is a stereo audio power amplifier in 24pin TSSOP thermal pad package. It can drive 1.8W continuous RMS power into 4Ω load per channel in Bridge-Tied Load (BTL) mode at 5V supply voltage. Its THD is smaller than 1% under the above operation condition. To simplify the audio system design in the notebook application, G1421 supports the Bridge-Tied Load (BTL) mode for driving the speakers, Single-End (SE) mode for driving the headphone. In the HP-IN mode, it can support a DC value to the phone-jacket and drive the headphone without the audio amplifier outputs coupling capacitors. G1421 can mute the output when Mute-In is activated. For the low current consumption applications, the SHDN mode is supported to disable G1421 when it is idle. The current consumption can be further reduced to below 5μA.

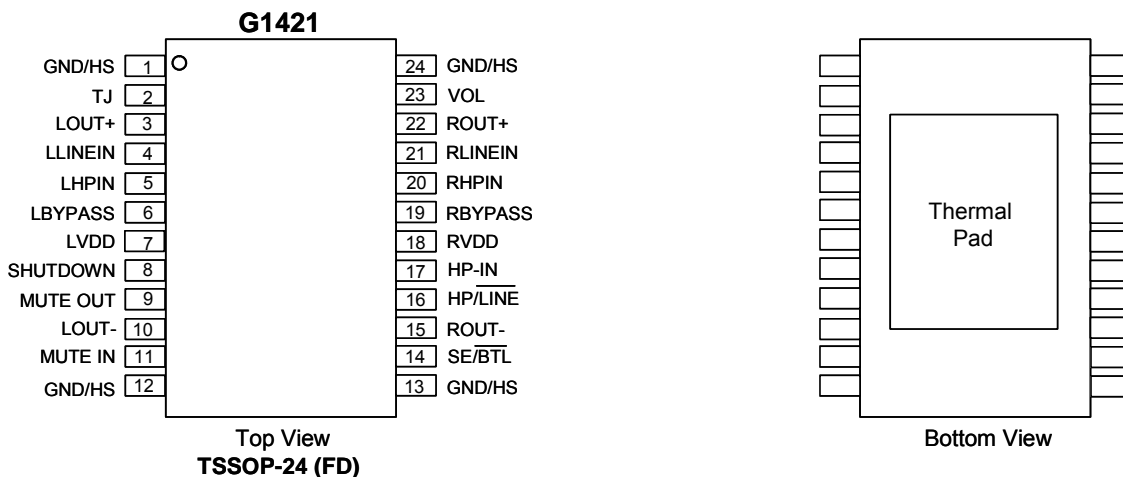
G1421 also supports two input paths, that means two different gain loops can be set in the same PCB and choosing either one by setting HP/LINE pin. It enhances the hardware designing flexibility. G1421 also supports an extra function -- the maximum output power clamping function to protect the speakers or headphones from burned-out.

### Ordering Information

ORDER NUMBER	ORDER NUMBER (Pb free)	TEMP. RANGE	PACKAGE
G1421	G1421f	-40°C to +85°C	TSSOP-24 (FD)

Note: U: Tape & Reel  
(FD): Thermal Pad

### Pin Configuration



Note: Recommend connecting the Thermal Pad to the GND for excellent power dissipation.

## Absolute Maximum Ratings

Supply Voltage, $V_{DD}$ .....6V	Power Dissipation <sup>(1)</sup>
Input Voltage, $V_I$ .....-0.3V to $V_{DD}+0.3V$	$T_A \leq 25^\circ\text{C}$ .....2.7W
Operating Ambient Temperature Range	$T_A \leq 70^\circ\text{C}$ .....1.7W
$T_A$ .....-40°C to +85°C	$T_A \leq 85^\circ\text{C}$ .....1.4W
Maximum Junction Temperature, $T_J$ .....150°C	Electrostatic Discharge, $V_{ESD}$
Storage Temperature Range, $T_{STG}$ .....-65°C to +150°C	Human body mode
Reflow Temperature (soldering, 10sec).....260°C	Lout- pin.....8000 to 8000V
	Other pins.....3000 to 3000 <sup>(2)</sup>

**Note:**

<sup>(1)</sup>: Recommended PCB Layout.

<sup>(2)</sup>: Human body model : C = 100pF, R = 1500Ω, 3 positive pulses plus 3 negative pulses

## Electrical Characteristics

### DC Electrical Characteristics, $T_A=+25^\circ\text{C}$

PARAMETER	SYMBOL	CONDITION	MIN	TYP	MAX	UNIT	
Supply Current	$I_{DD}$	$V_{DD} = 3.3V$ HP-IN	---	5.5	11	mA	
		$V_{DD} = 5V$ HP-IN	---	6.5	14		
		$V_{DD} = 3.3V$	Stereo BTL	---	7		13
			Stereo SE	---	3.5		8
		$V_{DD} = 5V$	Stereo BTL	---	8		16
Stereo SE	---		4	10			
DC Differential Output Voltage	$V_{O(DIFF)}$	$V_{DD} = 5V, \text{Gain} = 2$	---	5	50	mV	
Supply Current in Mute Mode	$I_{DD(MUTE)}$	$V_{DD} = 5V$	Stereo BTL	---	8	16	mA
			HP-IN	---	6.5	14	
			Stereo SE	---	4	10	
$I_{DD}$ in Shutdown	$I_{SD}$	$V_{DD} = 5V$	---	2	5	μA	

### (AC Operation Characteristics, $V_{DD} = 5.0V, T_A=+25^\circ\text{C}, R_L = 4\Omega$ , unless otherwise noted)

PARAMETER	SYMBOL	CONDITION	MIN	TYP	MAX	UNIT	
Output power (each channel) see Note	$P_{(OUT)}$	THD = 1%, BTL, $R_L = 4\Omega$	---	1.8	---	W	
		THD = 1%, BTL, $R_L = 8\Omega$	---	1.12	---		
		THD = 10%, BTL, $R_L = 4\Omega$	---	2	---		
		mW	$P_{(OUT)}$	THD = 10%, BTL, $R_L = 8\Omega$	---	1.4	---
				THD = 1%, SE, $R_L = 4\Omega$	---	500	---
				THD = 1%, SE, $R_L = 8\Omega$	---	320	---
				THD = 10%, SE, $R_L = 4\Omega$	---	650	---
				THD = 10%, SE, $R_L = 8\Omega$	---	400	---
Total harmonic distortion plus noise	THD+N	$P_O = 1.6W, \text{BTL}, R_L = 4\Omega$	---	500	---	m%	
		$P_O = 1W, \text{BTL}, R_L = 8\Omega$	---	150	---		
		$P_O = 75mW, \text{SE}, R_L = 32\Omega$	---	20	---		
		$V_I = 1V, R_L = 10K\Omega, G = 1$	---	10	---		
Maximum output power bandwidth	$B_{OM}$	$G = 1, \text{THD} = 1\%$	---	20	---	kHz	
Phase margin		$R_L = 4\Omega, \text{Open Load}$	---	60	---	°	
Power supply ripple rejection	PSRR	$f = 120\text{Hz}$	---	75	---	dB	
Mute attenuation			---	85	---	dB	
Channel-to-channel output separation		$f = 1\text{kHz}$	---	82	---	dB	
Line/HP input separation			---	80	---	dB	
BTL attenuation in SE mode			---	85	---	dB	
Input impedance	$Z_I$		---	2	---	MΩ	
Signal-to-noise ratio		$P_O = 500mW, \text{BTL}$	---	90	---	dB	
Output noise voltage	$V_n$	Output noise voltage	---	55	---	μV (rms)	

Note :Output power is measured at the output terminals of the IC at 1kHz.

(AC Operation Characteristics,  $V_{DD} = 3.3V$ ,  $T_A = +25^\circ C$ ,  $R_L = 4\Omega$ , unless otherwise noted)

PARAMETER	SYMBOL	CONDITION	MIN	TYP	MAX	UNIT
Output power (each channel) see Note	$P_{(OUT)}$	THD = 1%, BTL, $R_L = 4\Omega$	---	0.8	---	W
		THD = 1%, BTL, $R_L = 8\Omega$	---	0.5	---	
		THD = 10%, BTL, $R_L = 4\Omega$	---	1	---	
		THD = 10%, BTL, $R_L = 8\Omega$	---	0.6	---	
		THD = 1%, SE, $R_L = 4\Omega$	---	230	---	mW
		THD = 1%, SE, $R_L = 8\Omega$	---	140	---	
		THD = 10%, SE, $R_L = 4\Omega$	---	290	---	
		THD = 10%, SE, $R_L = 8\Omega$	---	180	---	
		THD = 0.5%, SE, $R_L = 32\Omega$	---	43	---	
Total harmonic distortion plus noise	THD+N	$P_O = 1.6W$ , BTL, $R_L = 4\Omega$	---	270	---	m%
		$P_O = 1W$ , BTL, $R_L = 8\Omega$	---	100	---	
		$P_O = 75mW$ , SE, $R_L = 32\Omega$	---	20	---	
		$V_I = 1V$ , $R_L = 10K\Omega$ , $G = 1$	---	10	---	
Maximum output power bandwidth	$B_{OM}$	$G = 1$ , THD 1%	---	20	---	kHz
Phase margin		$R_L = 4\Omega$ , Open Load	---	60	---	$^\circ$
Power supply ripple rejection	PSRR	$f = 120Hz$	---	75	---	dB
Mute attenuation			---	85	---	dB
Channel-to-channel output separation		$f = 1kHz$	---	80	---	dB
Line/HP input separation			---	80	---	dB
BTL attenuation in SE mode			---	85	---	dB
Input impedance	ZI		---	2	---	$M\Omega$
Signal-to-noise ratio		$P_O = 500mW$ , BTL	---	90	---	dB
Output noise voltage	$V_n$	Output noise voltage	---	55	---	$\mu V$ (rms)

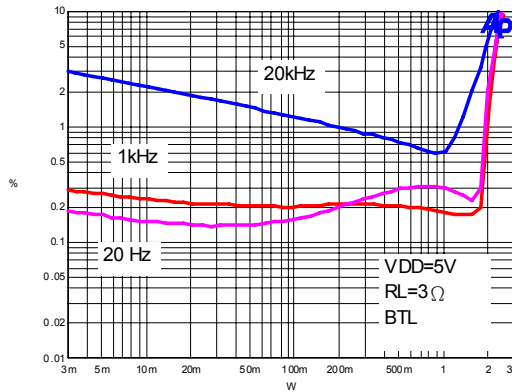
Note :Output power is measured at the output terminals of the IC at 1kHz.

**Typical Characteristics**

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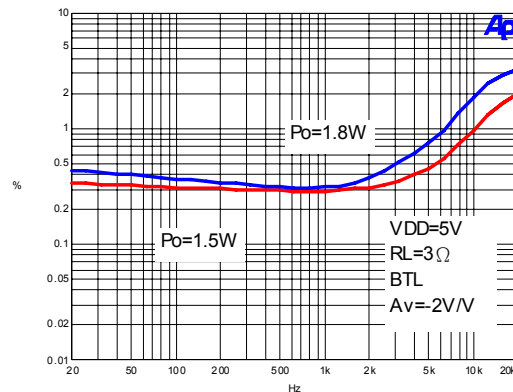
		<b>FIGURE</b>	
THD +N Total Harmonic Distortion Plus Noise	vs Output Power	1,3,6,9,10,13,16,19,22,25,26,27,33,36,39	
	vs Frequency	2,4,5,7,8,11,12,14,15,17,18,20,21,23,24,28,29,30,31,32,34,35,37,38,40,41	
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		vs Load Resistance	60,61
P <sub>D</sub>	Power Dissipation	vs Output Power	62,63,64,65

**Total Harmonic Distortion Plus Noise vs Output Power**



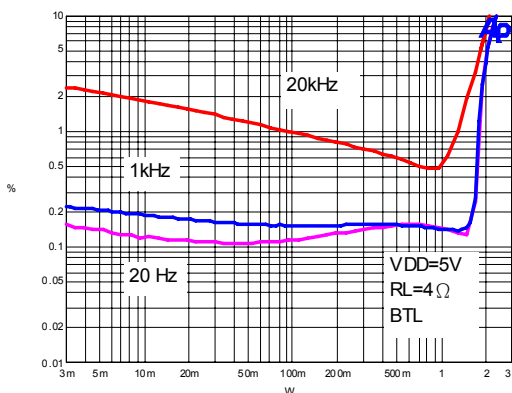
**Figure 1**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



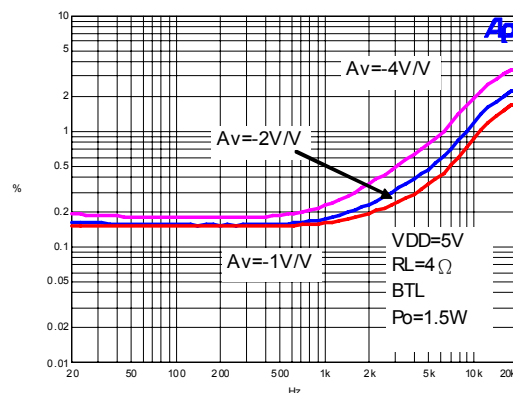
**Figure 2**

**Total Harmonic Distortion Plus Noise vs Output Power**



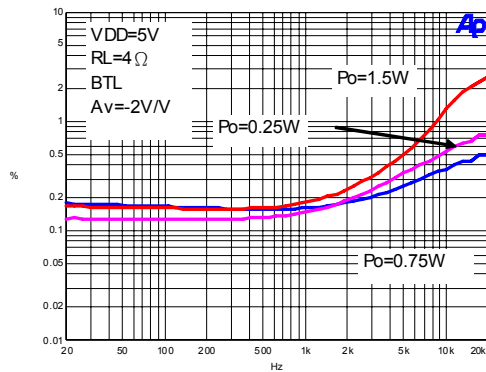
**Figure 3**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



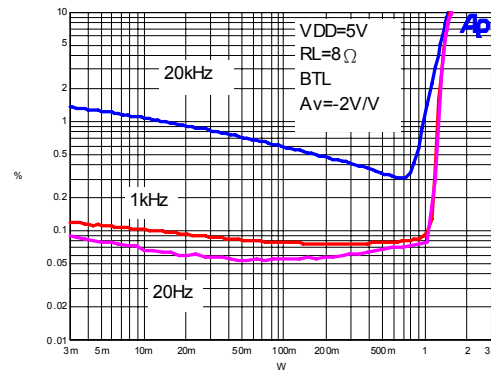
**Figure 4**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



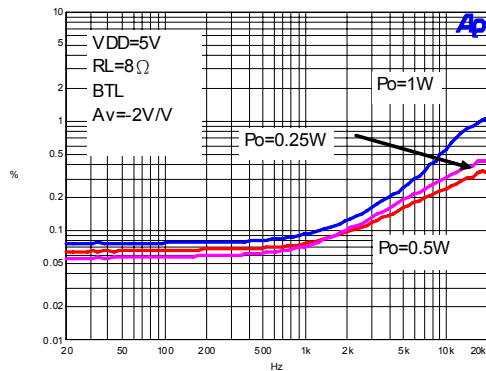
**Figure 5**

**Total Harmonic Distortion Plus Noise vs Output Power**



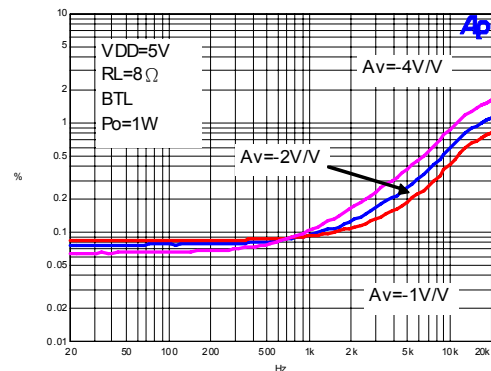
**Figure 6**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



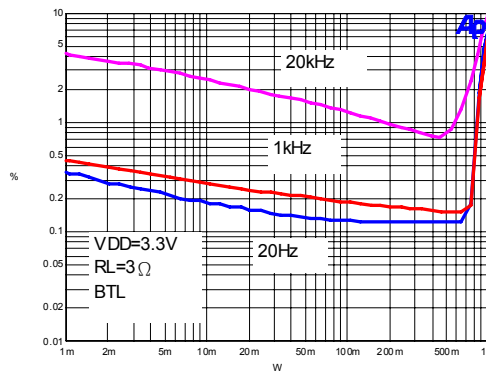
**Figure 7**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



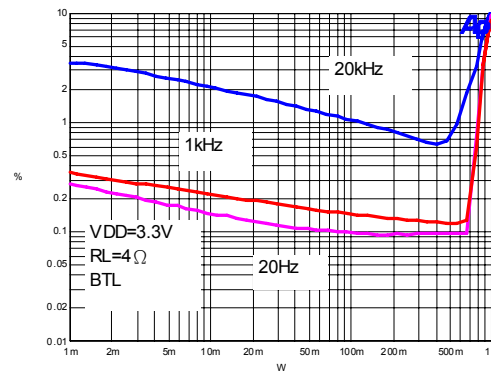
**Figure 8**

**Total Harmonic Distortion Plus Noise vs Output Power**



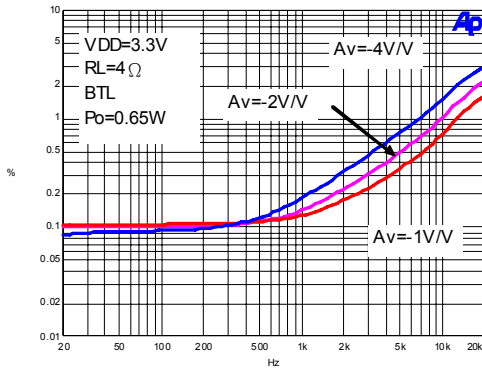
**Figure 9**

**Total Harmonic Distortion Plus Noise vs Output Power**



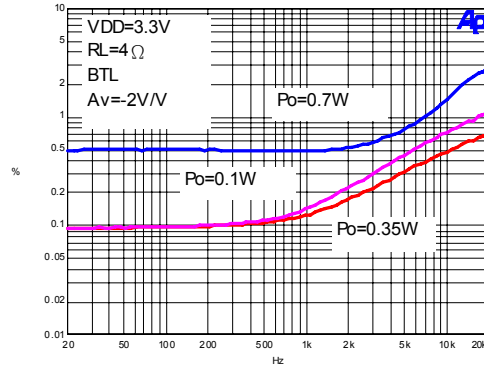
**Figure 10**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



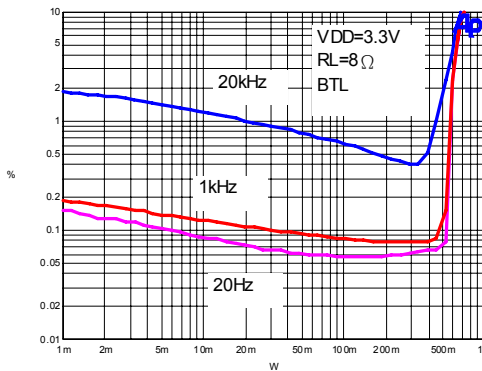
**Figure 11**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



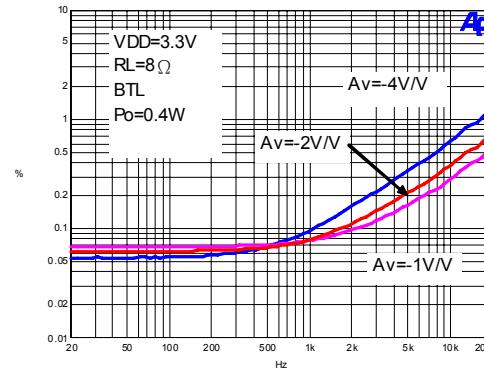
**Figure 12**

**Total Harmonic Distortion Plus Noise vs Output Power**



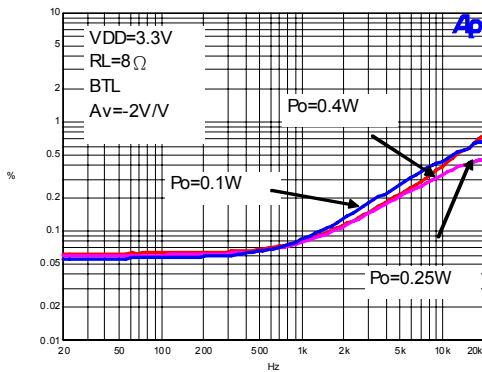
**Figure 13**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



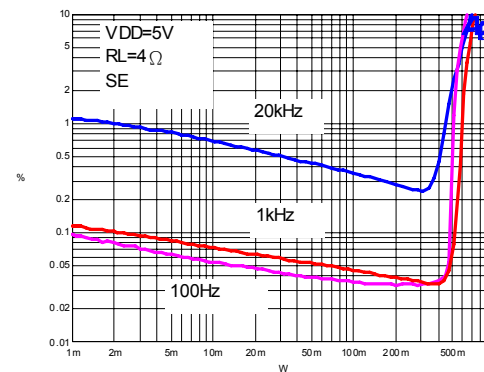
**Figure 14**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



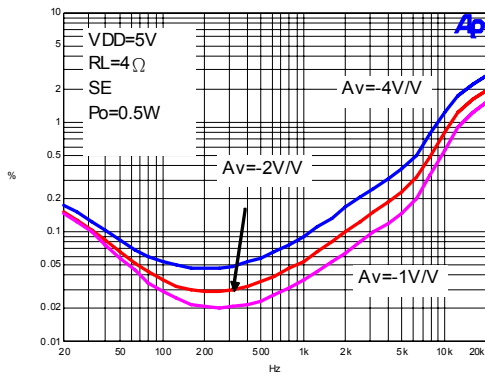
**Figure 15**

**Total Harmonic Distortion Plus Noise vs Output Power**



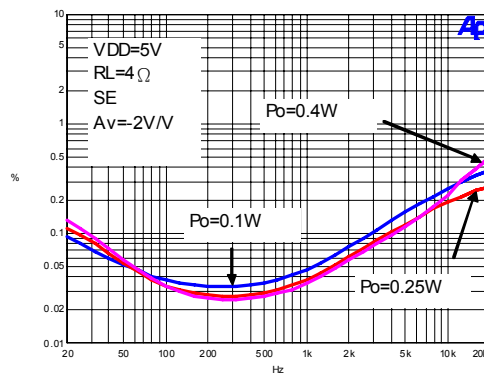
**Figure 16**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



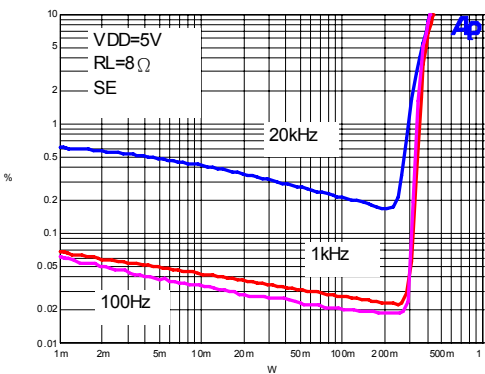
**Figure 17**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



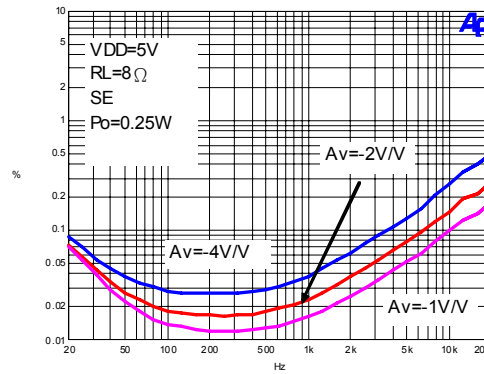
**Figure 18**

**Total Harmonic Distortion Plus Noise vs Output Power**



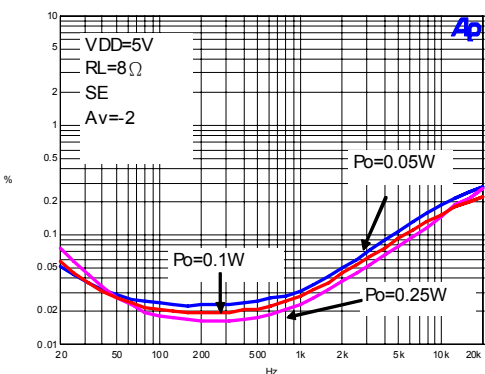
**Figure 19**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



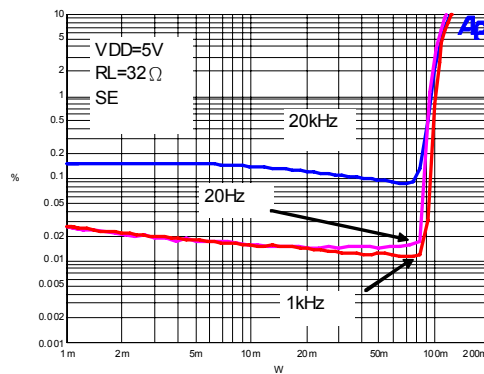
**Figure 20**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



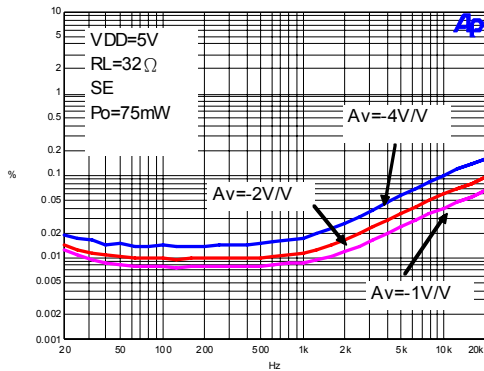
**Figure 21**

**Total Harmonic Distortion Plus Noise vs Output Power**



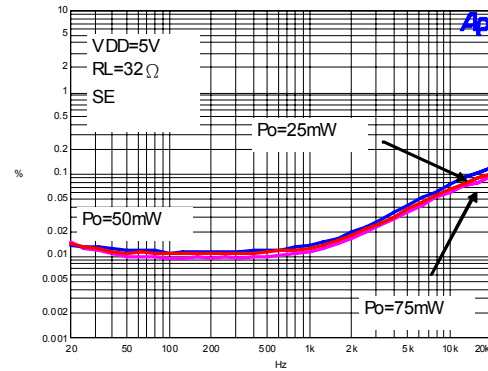
**Figure 22**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



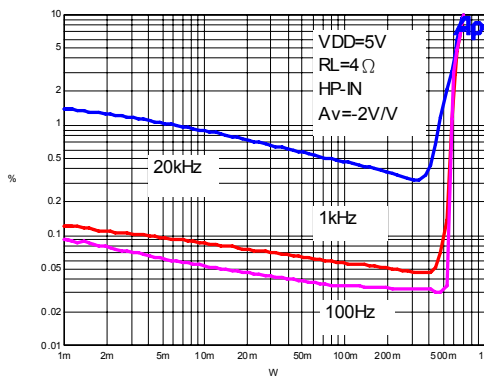
**Figure 23**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



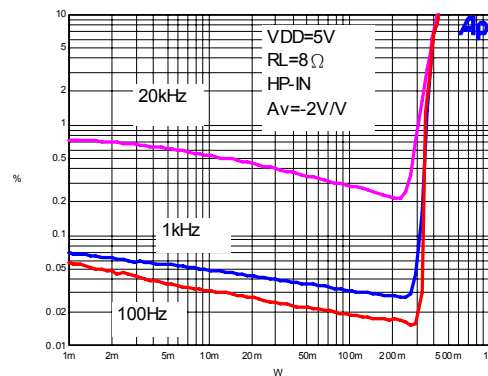
**Figure 24**

**Total Harmonic Distortion Plus Noise vs Output Power**



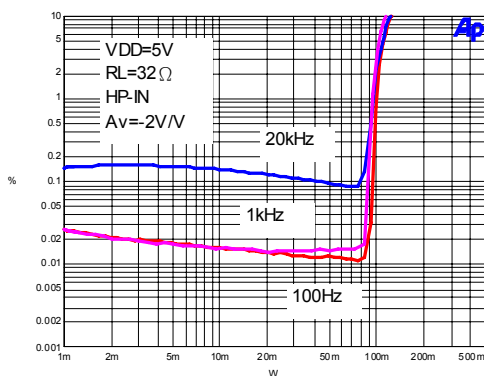
**Figure 25**

**Total Harmonic Distortion Plus Noise vs Output Power**



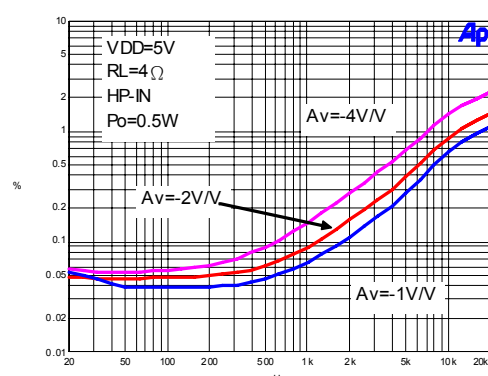
**Figure 26**

**Total Harmonic Distortion Plus Noise vs Output Power**



**Figure 27**

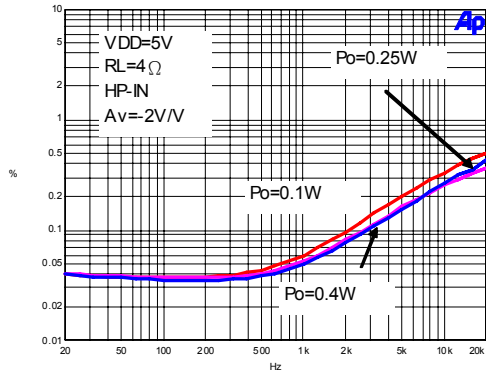
**Total Harmonic Distortion Plus Noise vs Output Power**



**Figure 28**

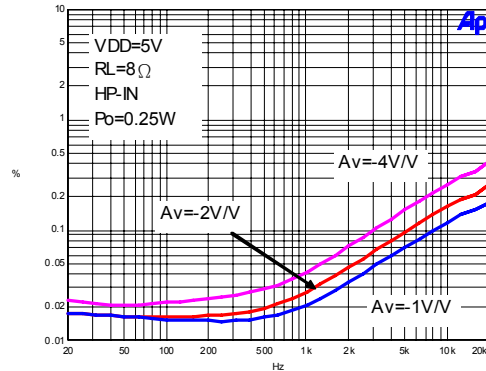


**Total Harmonic Distortion Plus Noise vs Output Frequency**



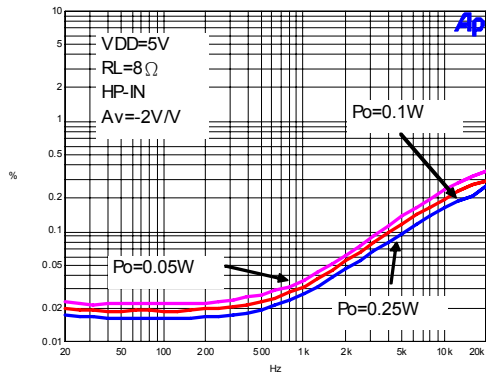
**Figure 29**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



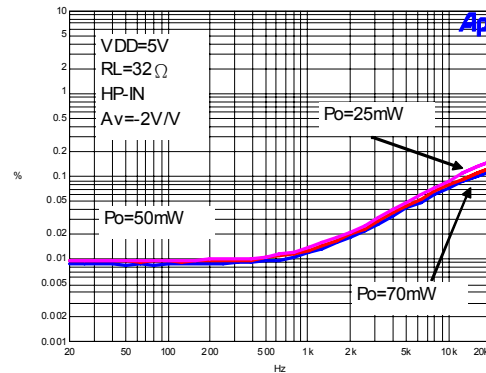
**Figure 30**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



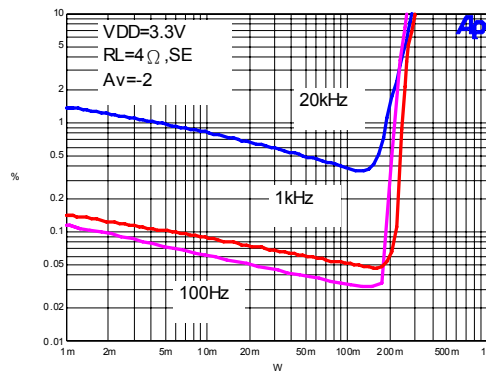
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**Total Harmonic Distortion Plus Noise vs Output Frequency**



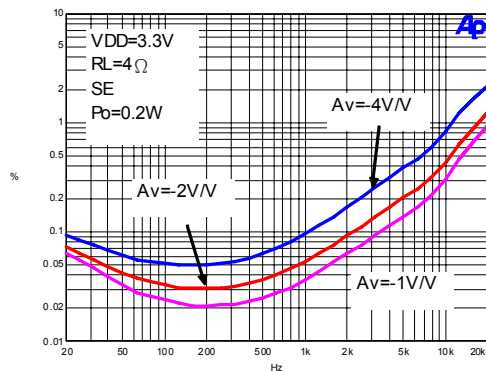
**Figure 32**

**Total Harmonic Distortion Plus Noise vs Output Power**



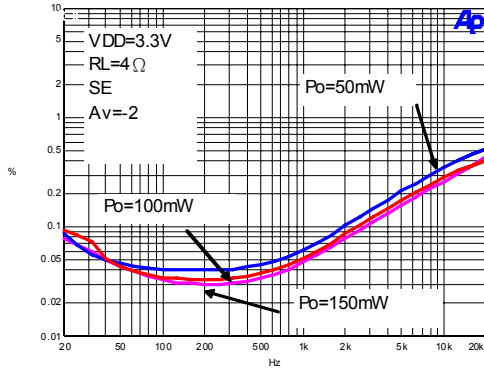
**Figure 33**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



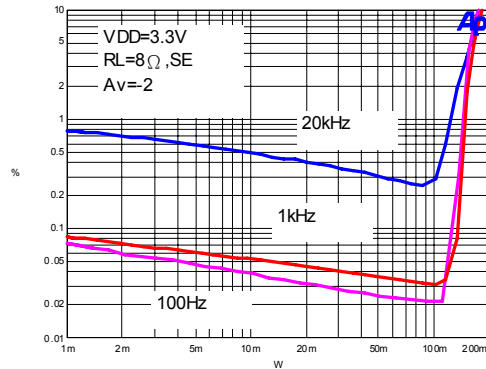
**Figure 34**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



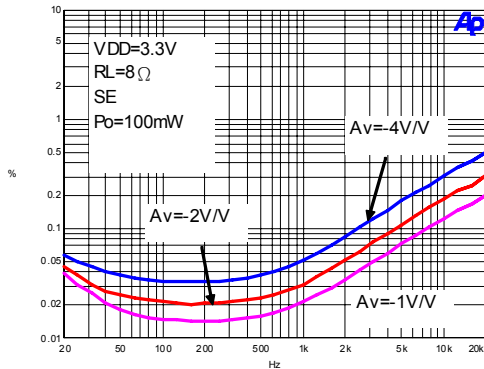
**Figure 35**

**Total Harmonic Distortion Plus Noise vs Output Power**



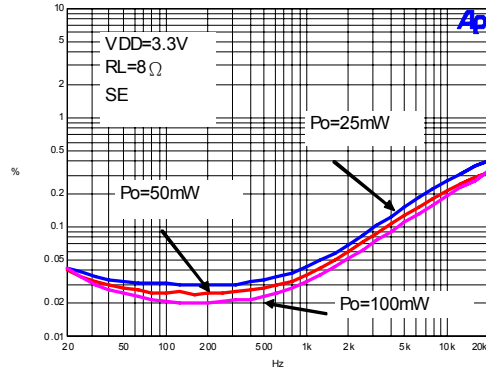
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**Total Harmonic Distortion Plus Noise vs Output Frequency**



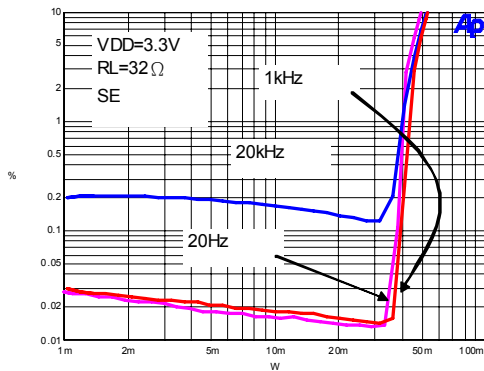
**Figure 37**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



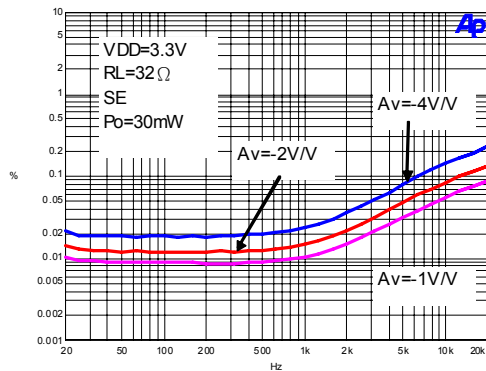
**Figure 38**

**Total Harmonic Distortion Plus Noise vs Output Power**



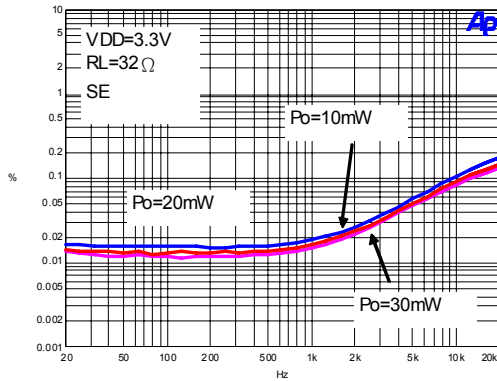
**Figure 39**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



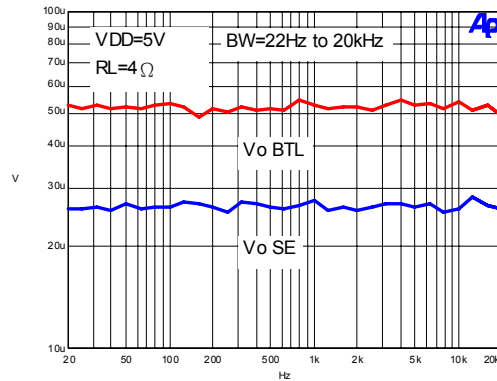
**Figure 40**

**Total Harmonic Distortion Plus Noise vs Output Frequency**



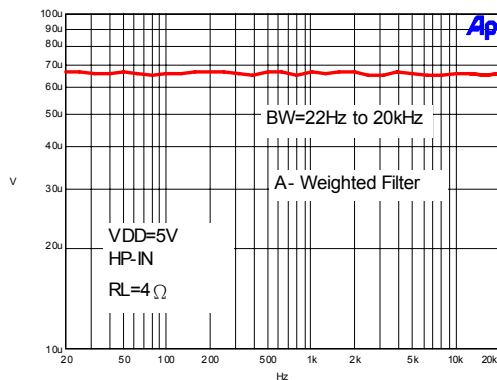
**Figure 41**

**Output Noise Voltage vs Frequency**



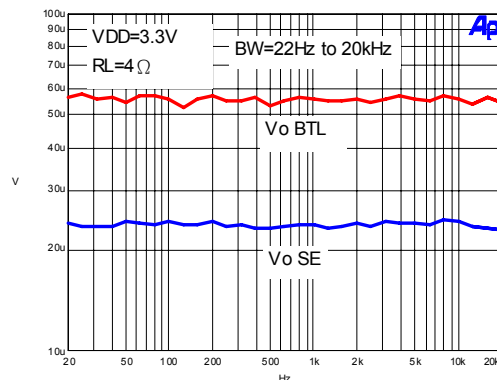
**Figure 42**

**Output Noise Voltage vs Frequency**



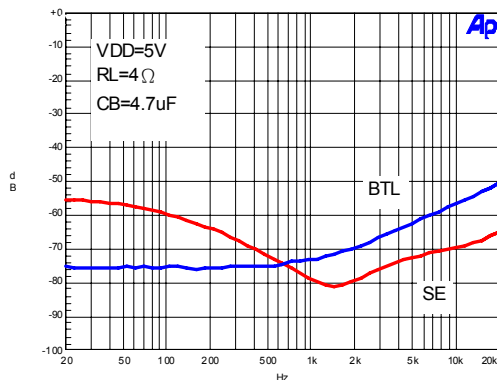
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**Output Noise Voltage vs Frequency**



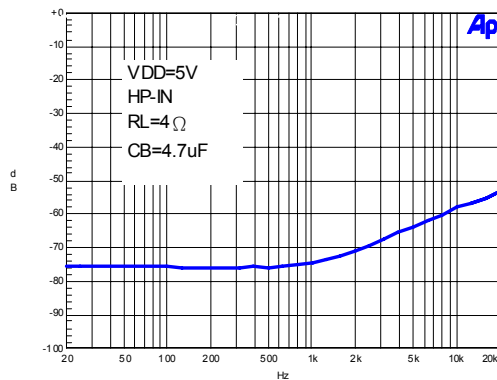
**Figure 44**

**Supply Ripple Rejection Ratio vs Frequency**



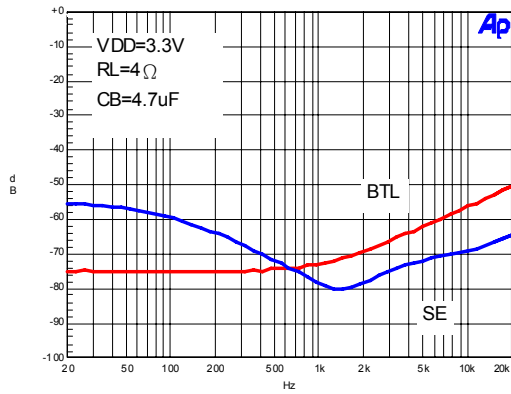
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**Supply Ripple Rejection Ratio vs Frequency**



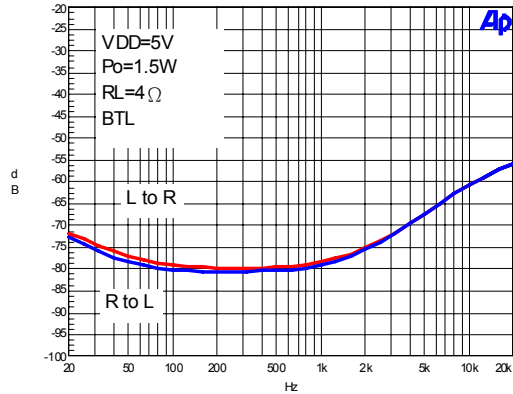
**Figure 46**

**Supply Ripple Rejection Ratio vs Frequency**



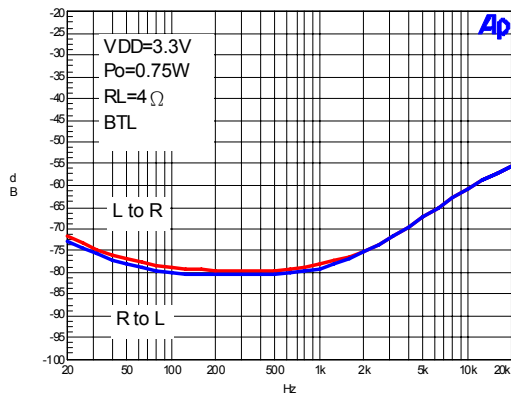
**Figure 47**

**Crosstalk vs Frequency**



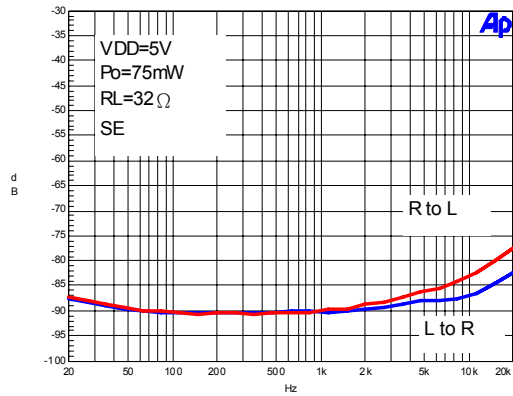
**Figure 48**

**Crosstalk vs Frequency**



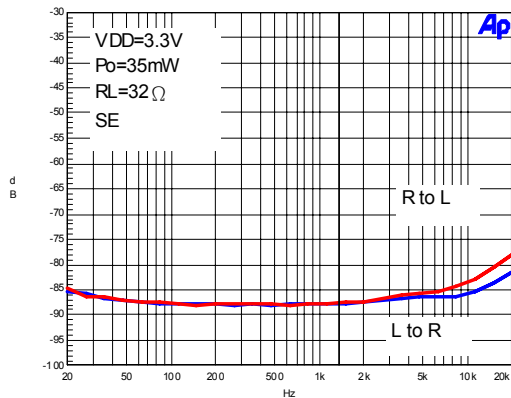
**Figure 49**

**Crosstalk vs Frequency**



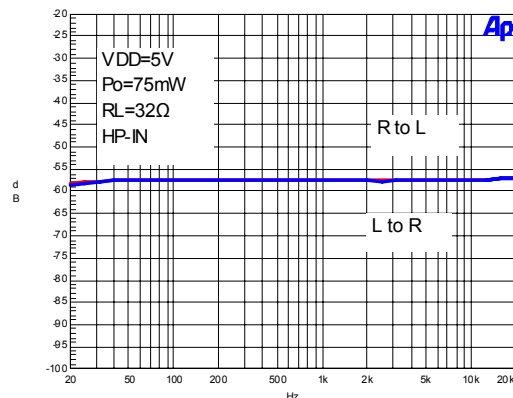
**Figure 50**

**Crosstalk vs Frequency**



**Figure 51**

**Crosstalk vs Frequency**



**Figure 52**

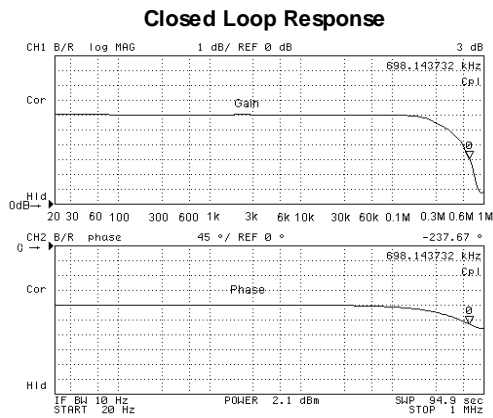


Figure 53

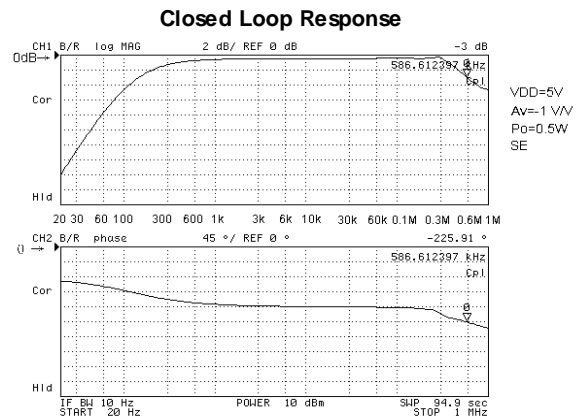


Figure 54

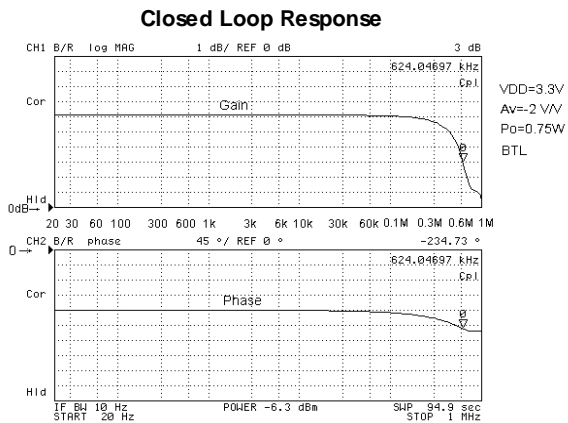


Figure 55

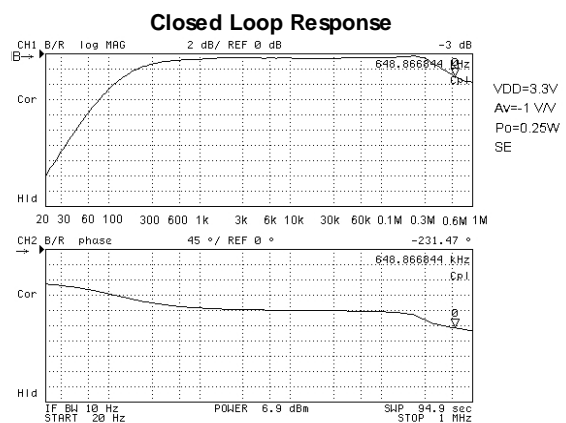


Figure 56

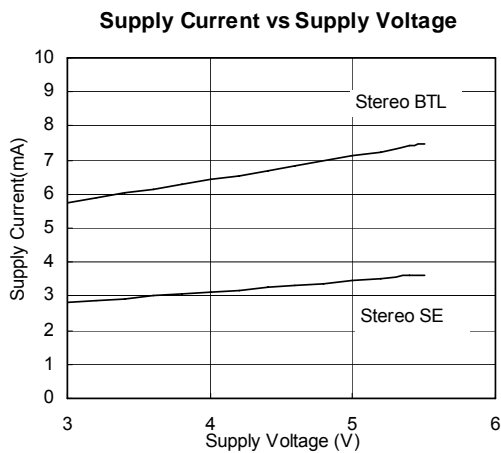


Figure 57

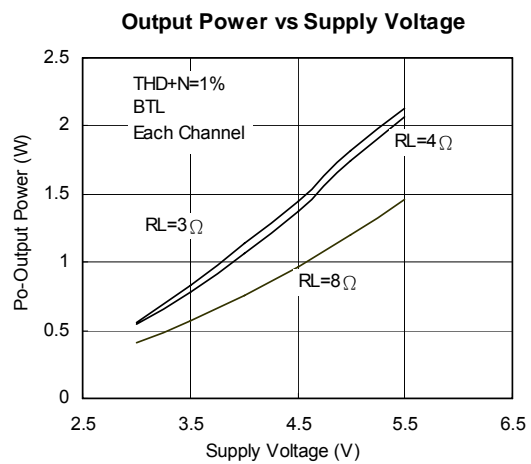
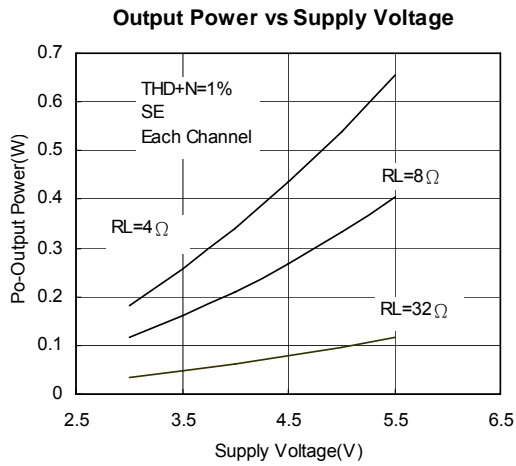
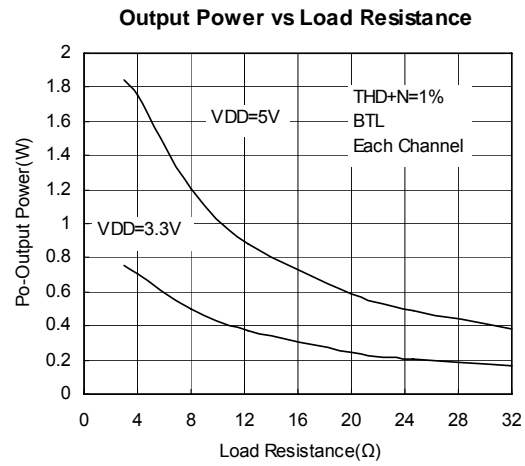


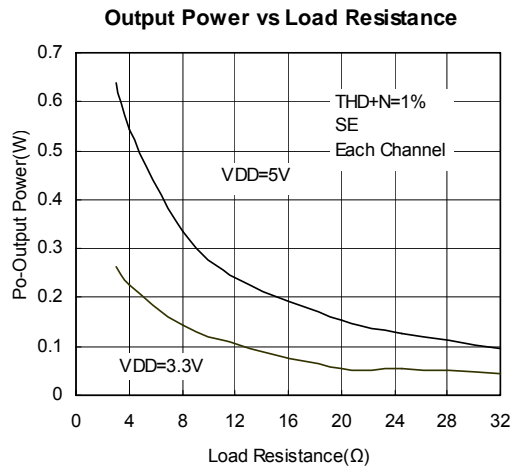
Figure 58



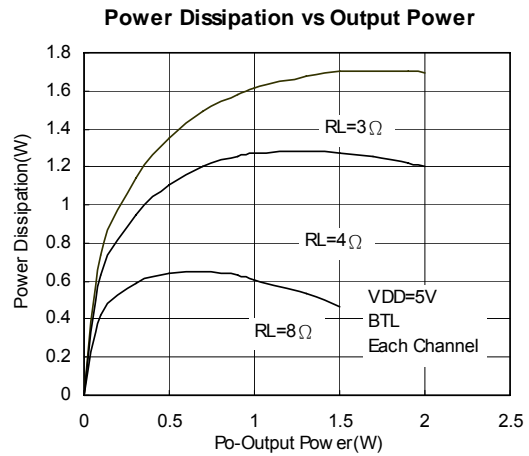
**Figure 59**



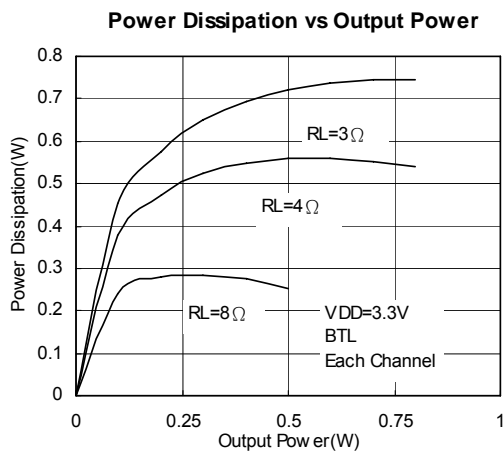
**Figure 60**



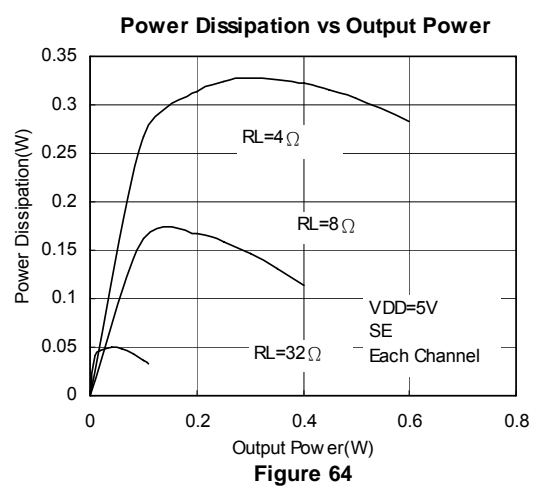
**Figure 61**



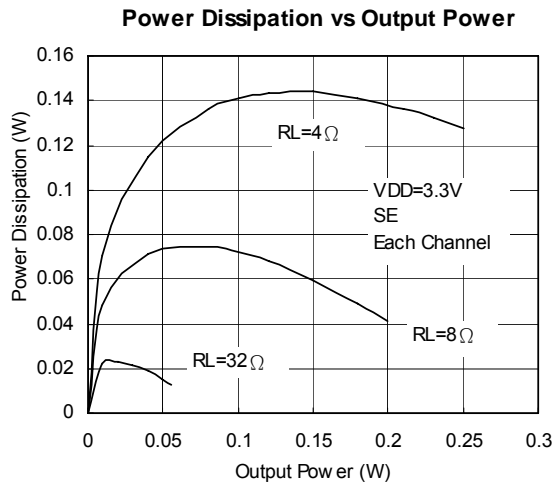
**Figure 62**



**Figure 63**

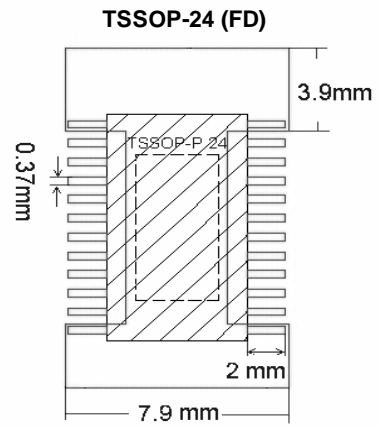


**Figure 64**



**Figure 65**

**Recommended Minimum Footprint**

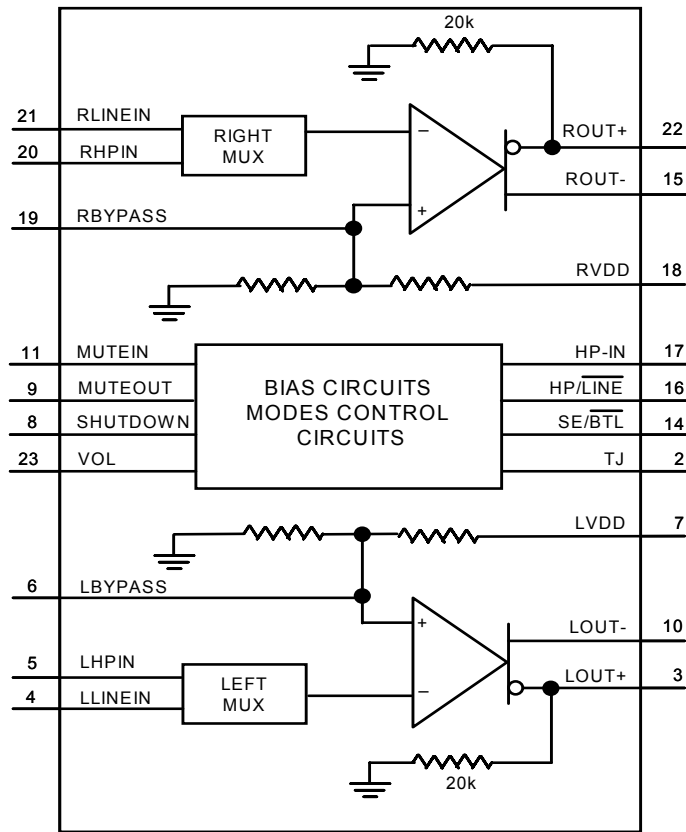


## Pin Description

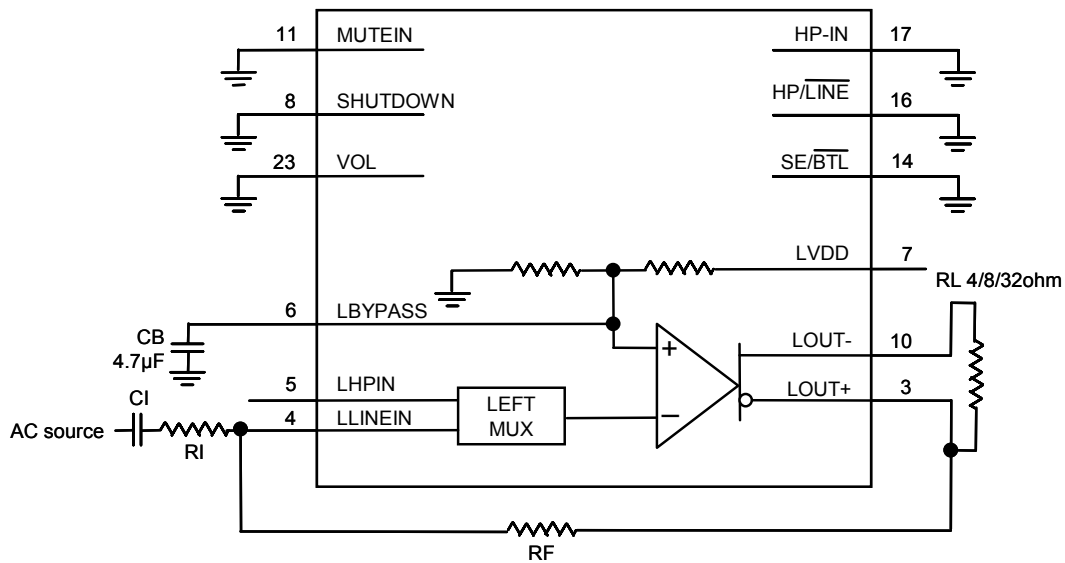
PIN	NAME	I/O	FUNCTION
1,12,13,24	GND/HS		Ground connection for circuitry, directly connected to thermal pad.
2	TJ	O	Source a current inversely to the junction temperature. This pin should be left unconnected during normal operation. For more information, see the junction temperature measurement section of this document.
3	LOUT+	O	Left channel + output in BTL mode, + output in SE mode.
4	LLINE IN	I	Left channel line input, selected when HP/ pin is held low.
5	LHP IN	I	Left channel headphone input, selected when HP/pin is held high.
6	LBYPASS		Connect to voltage divider for left channel internal mid-supply bias.
7	LVDD	I	Supply voltage input for left channel and for primary bias circuits.
8	SHUTDOWN	I	Shutdown mode control signal input, places entire IC in shutdown mode when held high, $I_{DD} = 5\mu A$ .
9	MUTE OUT	O	Follows MUTE IN pin, provides buffered output.
10	LOUT-	O	Left channel - output in BTL mode, high impedance state in SE mode. Supply $V_{DD}/2$ to the phone jacket in HP-IN mode.
11	MUTE IN	I	Mute control signal input, hold low for normal operation, hold high to mute.
14	SE/	I	Mode control signal input, hold low for BTL mode, hold high for SE mode.
15	ROUT-	O	Right channel - output in BTL mode, high impedance state in SE mode.
16	HP/	I	MUX control input, hold high to select headphone inputs (5,20), hold low to select line inputs (4,21).
17	HP-IN		This pin can activate the HP-IN mode to supplied the $V_{DD}/2$ at LOUT- onto the phone jacket. So the DC blocking capacitors can be removed in HP-IN type (like SE mode except no DC blocking capacitors). Hold high to activate this function. If this function is not used, it should be strongly tied to low.
18	RVDD	I	Supply voltage input for right channel.
19	RBYPASS		Connect to voltage divider for right channel internal mid-supply bias.
20	RHP IN	I	Right channel headphone input, selected when HP/pin is held high.
21	RLINE IN	I	Right channel line input, selected when HP/pin is held low.
22	ROUT+	O	Right channel + output in BTL mode, + output in SE mode.
23	VOL	I	The output power can be clamped by setting a low bound voltage to this pin. The high bound voltage will be generated internally. The output voltage will be clamped between high/low bound voltages. Then the output power is limited. It is weakly pull-low internally, let this pin floating or tied to GND can deactivate this function.
Thermal Pad			Recommend connecting the Thermal Pad to the GND for excellent power dissipation.



**Block Diagram**

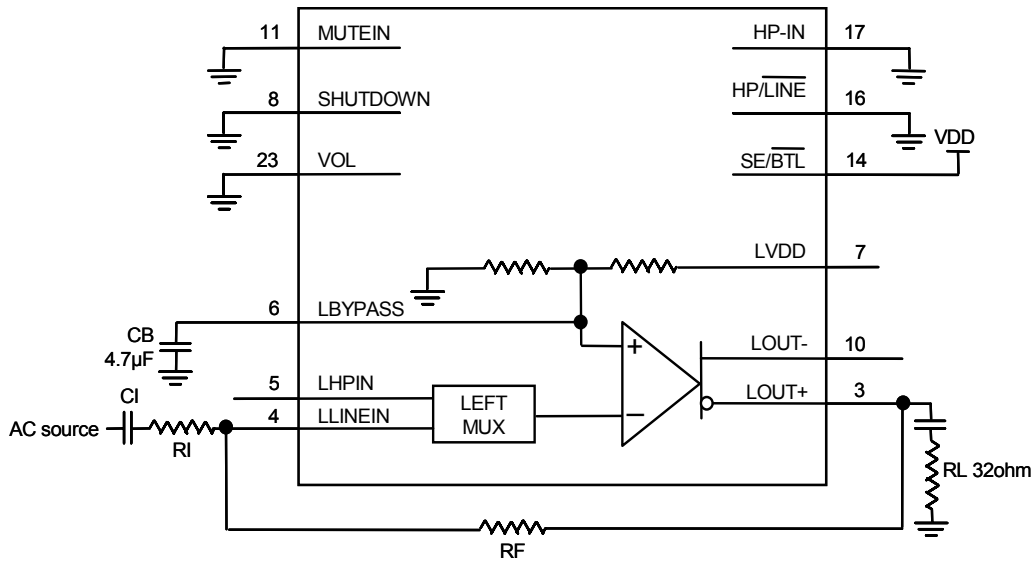


**Parameter Measurement Information**

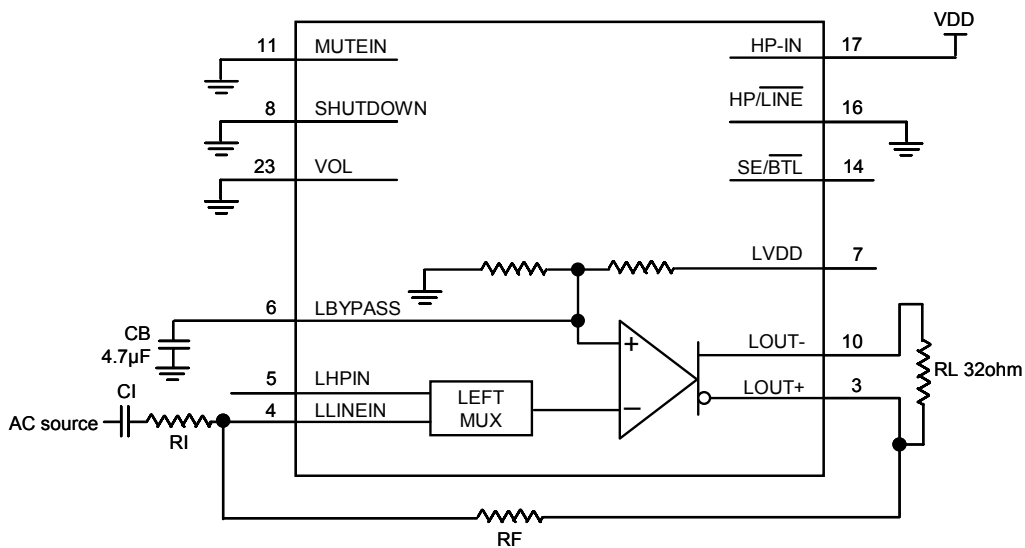


**BTL Mode Test Circuit**

Parameter Measurement Information (Continued)



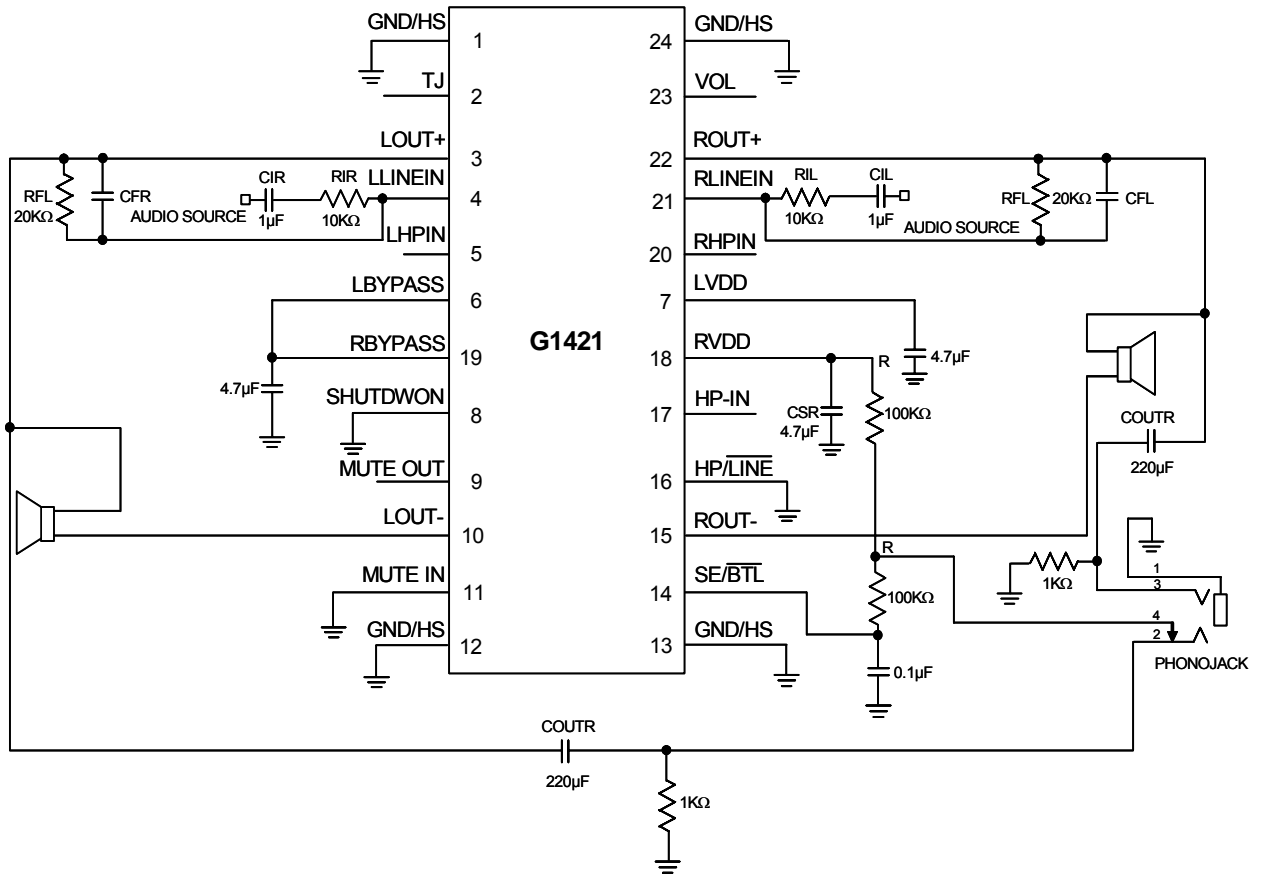
**SE Mode Test Circuit**



**HP-IN Mode (Non-DC Blocking Cap) Test Circuit**

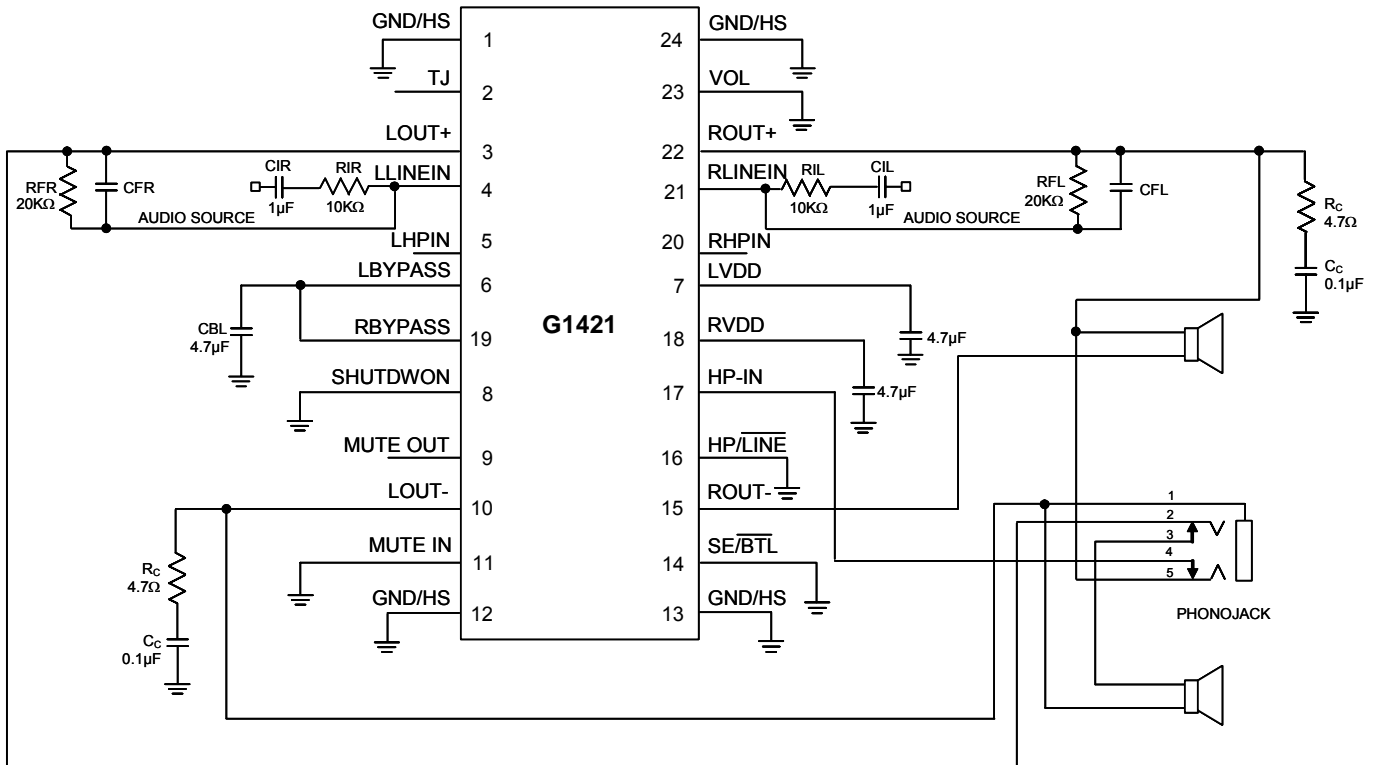
**Application Circuits**

**With DC blocking Capacitors Application**



## Application Circuits (Continued)

### No DC Blocking Capacitors Application



### Logical Truth Table

INPUTS					OUTPUT	AMPLIFIER STATES				
SE/BTL	HP/LINE	HP-IN	Mute In	Shutdown	Mute Out	Input	L/R Out+	L Out-	R Out-	Mode
X	X	X	---	High	---	X	---	---	---	Mute
Low	X	X	High	---	High	X	VDD/2	VDD/2	VDD/2	Mute
High	X	X	High	---	High	X	VDD/2	---	---	Mute
X	X	High	High	---	High	X	VDD/2	VDD/2	---	Mute
Low	Low	Low	Low	Low	Low	L/R Line	BTL Output	BTL Output	BTL Output	BTL
Low	High	Low	Low	Low	Low	L/R HP	BTL Output	BTL Output	BTL Output	BTL
High	Low	Low	Low	Low	Low	L/R Line	SE Output	---	---	SE
High	High	Low	Low	Low	Low	L/R HP	SE Output	---	---	SE
X	Low	High	Low	Low	Low	L/R Line	SE Output	VDD/2	---	HP-IN
X	High	High	Low	Low	Low	L/R HP	SE Output	VDD/2	---	HP-IN

**Application Information**

**Input MUX Operation**

There are two input signal paths – HP & Line. With the prompt setting, G1421 allows the setting of different gains for BTL and SE modes. Generally, speakers typically require approximately a factor of 10 more gain for similar volume listening levels as compared with headphones.

$$\text{SE Gain}_{(\text{HP})} = -(R_{\text{F}(\text{HP})}/R_{\text{I}(\text{HP})})$$

$$\text{BTL Gain}_{(\text{LINE})} = -2(R_{\text{F}(\text{LINE})}/R_{\text{I}(\text{LINE})})$$

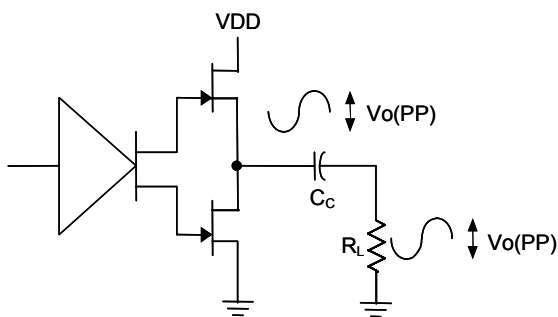
To achieve headphones and speakers listening parity,  $(R_{\text{F}(\text{LINE})}/R_{\text{I}(\text{LINE})})$  is suggested to be 5 times of  $(R_{\text{F}(\text{HP})}/R_{\text{I}(\text{HP})})$ . The ratio of  $(R_{\text{F}(\text{HP})}/R_{\text{I}(\text{HP})})$  can be determined by the applications. When the optimum distortion performance into the headphones (clear sound) is important, gain of  $-1$  ( $(R_{\text{F}(\text{HP})}/R_{\text{I}(\text{HP})}) = 1$ ) is suggested.

**Single Ended Mode Operation**

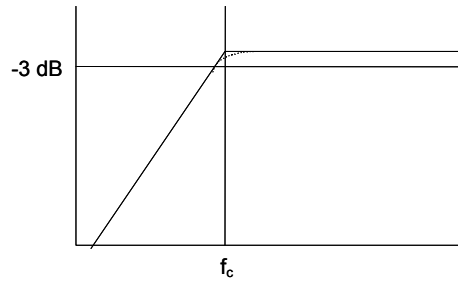
G1421 can drive clean, low distortion SE output power into headphone loads (generally  $16\Omega$  or  $32\Omega$ ) as in Figure A. Please refer to **Electrical Characteristics** to see the performances. A coupling capacitor is needed to block the dc offset voltage, allowing pure ac signals into headphone loads. Choosing the coupling capacitor will also determine the 3 dB point of the high-pass filter network, as Figure B.

$$f_c = 1/(2\pi R_L C_C)$$

For example, a  $68\mu\text{F}$  capacitor with  $32\Omega$  headphone load would attenuate low frequency performance below  $73\text{Hz}$ . So the coupling capacitor should be well chosen to achieve the excellent bass performance when in SE mode operation.



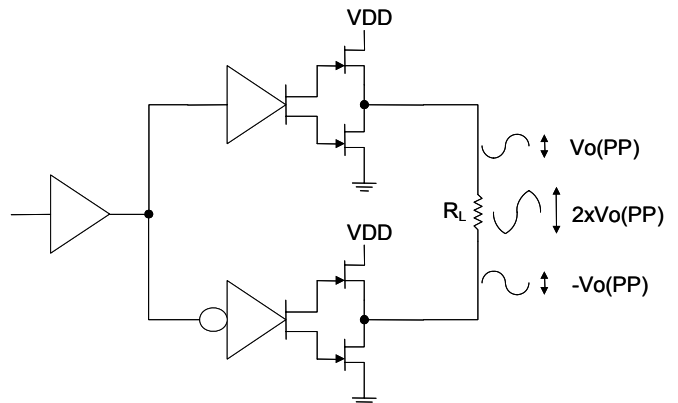
**Figure A**



**Figure B**

**Bridged-Tied Load Mode Operation**

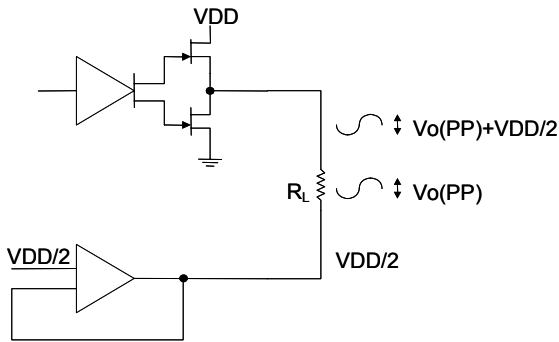
G1421 has two linear amplifiers to drive both ends of the speaker load in Bridged-Tied Load (BTL) mode operation. Figure C shows the BTL configuration. The differential driving to the speaker load means that when one side is slewing up, the other side is slewing down, and vice versa. This configuration in effect will double the voltage swing on the load as compared to a ground reference load. In BTL mode, the peak-to-peak voltage  $V_o(\text{PP})$  on the load will be two times than a ground reference configuration. The voltage on the load is doubled, this will also yield 4 times output power on the load at the same power supply rail and loading. Another benefit of using differential driving configuration is that BTL operation cancels the dc offsets, which eliminates the dc coupling capacitor that is needed to cancelled dc offsets in the ground reference configuration. Low-frequency performance is then limited only by the input network and speaker responses. Cost and PCB space can be minimized by eliminating the dc coupling capacitors.



**Figure C**

**HP-IN Mode Operation**

An internal weakly pull-up circuit is connected to HP-IN control pin (pin 17). When this pin is left unconnected or tied to VDD, HP-IN mode is activated, ignoring SE/  $\overline{\text{BTL}}$  setting. In normal SE/  $\overline{\text{BTL}}$  mode operations, this HP-IN pin should be tied to GND. In HP-IN mode, the linear amplifiers of LOUT+ (pin 3) /ROUT+ (pin 22) are still alive, the linear amplifier of ROUT- (pin 15) is deactivated, the linear amplifier of LOUT- (pin 10) supplies VDD/2 on this pin to cancel the dc offsets. (Please refer to Logical Truth Table and No DC CAP Application Circuit for detailed operation.) If connected VDD/2 on the LOUT- (pin 10) to the phone jacket, the dc offset can be eliminated without using coupling capacitors in headphone applications. By using HP-IN mode, cost and PCB space can be further minimized than traditional headphone applications with coupling capacitors. The HP-IN configuration is shown on Figure D.



**Figure D**

Short circuit protection is implemented on LOUT- (pin10) to avoid the short-circuit damage caused by the sleeve of the phone jack connected to ground accidentally during the module assembling. When short-circuit is detected, the linear amplifier of LOUT- (pin 10) will turn off for a period. After this period, it activates again. If the short circuit condition still exists, it will be turned off again. With this protection, the damage caused by larger dc short circuit current (from VDD/2 to GND) can be avoided.

**MUTE and SHUTDOWN Mode Operations**

G1421 implements the mute and shutdown mode operations to reduce supply current,  $I_{DD}$ , to the absolute minimum level during nonuse periods for battery-power conservation. When the shutdown pin (pin 8) is pulled high, all linear amplifiers will be deactivated to mute the amplifier outputs. And G1421 enters an extra low current consumption state,  $I_{DD}$  is smaller than  $5\mu\text{A}$ . If pulling mute-in pin (pin 11) high, it will force the activated linear amplifier to supply the VDD/2 dc voltage on the output to mute the AC performance. In mute mode operation, the current consumption will be a little different between BTL, SE and HP-IN modes. (SE < HP-IN < BTL) Typically, the supply current is about 2.5mA in BTL mute operation. Shutdown and Mute-In pins should never be left unconnected, this floating condition will cause the amplifier operations unpredictable.

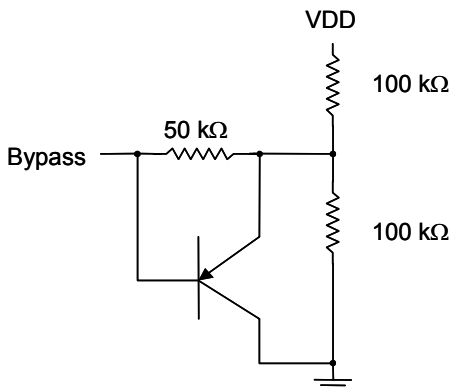
**Maximum Power Clamping Function**

G1421 supports the maximum output power clamping function to avoid damaging the speaker when the amplifier output a power beyond the speaker tolerance. The Vol pin (pin 23) is weakly pull-low internally. If inputting a non-zero voltage (low boundary voltage) to the Vol pin, G1421 will generate a high boundary voltage which the difference between the VDD/2 and the high boundary voltage is the same as the difference between the VDD/2 and the low boundary voltage. ( i.e.  $V_{OH} - VDD/2 = VDD/2 - V_{OL}$  ) Then the outputs of linear amplifiers will be effectively limited between the high/low boundary voltage, the maximum output power is clamped. By setting the voltage of Vol, the maximum output power can be well controlled. When the maximum power clamping function is not used, the Vol pin should be floated or tied to GND.

**Optimizing DEPOP Operation**

Circuitry has been implemented in G1421 to minimize the amount of popping heard at power-up and when coming out of shutdown mode. Popping occurs whenever a voltage step is applied to the speaker and making the differential voltage generated at the two ends of the speaker. To avoid the popping heard, the bypass capacitor should be chosen promptly,  $1/(C_B \times 100k\Omega) \leq 1/(C_I \times (R_I + R_F))$ . Where  $100k\Omega$  is the output impedance of the mid-rail generator,  $C_B$  is the mid-rail bypass capacitor,  $C_I$  is the input coupling capacitor,  $R_I$  is the input impedance,  $R_F$  is the gain setting impedance which is on the feedback path.  $C_B$  is the most important capacitor. Besides it is used to reduce the popping,  $C_B$  can also determine the rate at which the amplifier starts up during startup or recovery from shutdown mode.

De-popping circuitry of G1421 is shown on Figure E. The PNP transistor limits the voltage drop across the  $50k\Omega$  by slewing the internal node slowly when power is applied. At start-up, the voltage at BYPASS capacitor is 0. The PNP is ON to pull the mid-point of the bias circuit down. So the capacitor sees a lower effective voltage, and thus the charging is slower. This appears as a linear ramp (while the PNP transistor is conducting), followed by the expected exponential ramp of an R-C circuit.

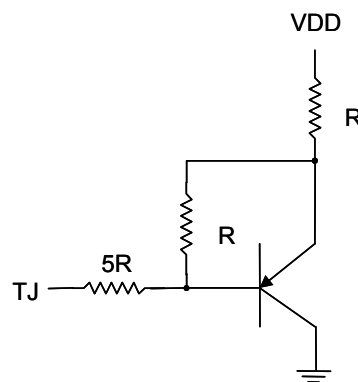


**Figure E**

**Junction Temperature Measurement**

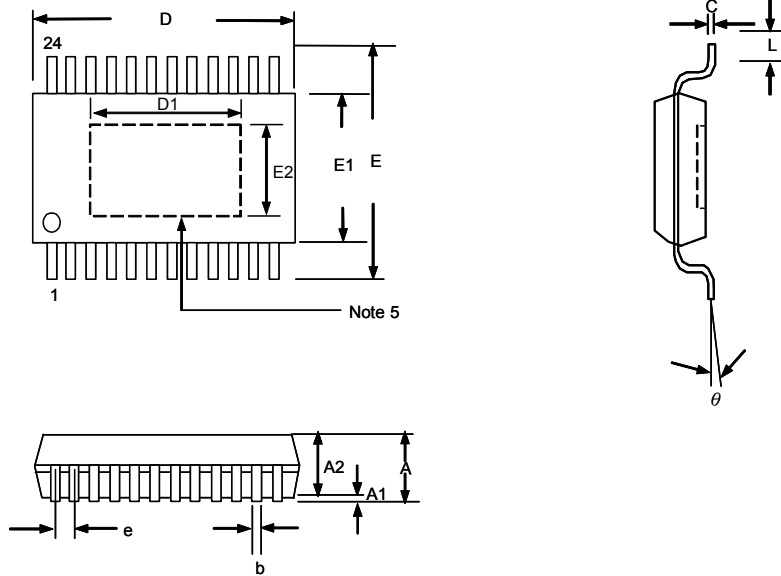
Characterizing a PCB layout with respect to thermal impedance is very difficult, as it is usually impossible to know the junction temperature of the IC. G1421 TJ (pin 2) sources a current inversely proportional to the junction temperature. Typically TJ sources  $-120\mu A$  for a 5V supply at  $25^\circ C$ . And the slope is approximately  $0.22\mu A/^\circ C$ . As the resistors have a tolerance of  $\pm 20\%$ , these values should be calibrated on each device. When the temperature sensing function is not used, TJ pin can be left floating or tied to VDD to reduce the current consumption.

Temperature sensing circuit is shown on Figure F.



**Figure F**

## Package Information



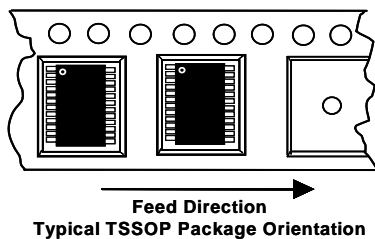
**TSSOP-24(FD) Package**

**NOTE:**

1. Package body sizes exclude mold flash protrusions or gate burrs
2. Tolerance  $\pm 0.1\text{mm}$  unless otherwise specified
3. Coplanarity : 0.1mm
4. Controlling dimension is millimeter. Converted inch dimensions are not necessarily exact.
5. Die pad exposure size is according to lead frame design.
6. Follow JEDEC MO-153

SYMBOLS	DIMENSION IN MM			DIMENSION IN INCH		
	MIN	NOM	MAX	MIN	NOM	MAX
A	----	----	1.20	----	----	0.047
A1	0.00	----	0.15	0.000	----	0.006
A2	0.80	1.00	1.05	0.031	0.039	0.041
b	0.19	----	0.30	0.007	----	0.012
C	0.20	----	----	0.008	----	----
D	7.7	7.8	7.9	0.303	0.307	0.311
D1	4.4	----	4.9	0.173	----	0.193
E	6.40 BSC			0.252 BSC		
E1	4.30	4.40	4.50	0.169	0.173	0.177
E2	2.7	----	3.2	0.106	----	0.126
e	0.65 BSC			0.026 BSC		
L	0.45	0.60	0.75	0.018	0.024	0.030
$\theta$	0°	----	8°	0°	----	8°

## Taping Specification



PACKAGE	Q'TY/REEL
TSSOP-24 (FD)	2,500 ea

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