

IRFR3707Z IRFU3707Z

KERSEMI ELECTRONIC CO.,LTD.

Applications

- High Frequency Synchronous Buck Converters for Computer Processor Power
- High Frequency Isolated DC-DC Converters with Synchronous Rectification for Telecom and Industrial Use

D-Pak IRFR3707Z I-Pak IRFU3707Z





Benefits

- Very Low R_{DS(on)} at 4.5V V_{GS}
- Ultra-Low Gate Impedance
- Fully Characterized Avalanche Voltage and Current

V_{DSS}	R _{DS(on)} max	Qg
30V	9.5m $Ω$	9.6nC

Absolute Maximum Ratings

	Parameter	Max.	Units	
V_{DS}	Drain-to-Source Voltage	30	V	
V_{GS}	Gate-to-Source Voltage	± 20		
$I_D @ T_C = 25^{\circ}C$	Continuous Drain Current, V _{GS} @ 10V	56④	А	
I _D @ T _C = 100°C	Continuous Drain Current, V _{GS} @ 10V	394		
I _{DM}	Pulsed Drain Current ①	220		
P _D @T _C = 25°C	Maximum Power Dissipation	50	W	
P _D @T _C = 100°C	Maximum Power Dissipation	25		
	Linear Derating Factor	0.33	W/°C	
T _J	Operating Junction and	-55 to + 175	°C	
T _{STG}	Storage Temperature Range			
	Soldering Temperature, for 10 seconds	300 (1.6mm from case)		

Thermal Resistance

	Parameter	Тур.	Max.	Units
$R_{\theta JC}$	Junction-to-Case		3.0	°C/W
$R_{\theta JA}$	Junction-to-Ambient (PCB Mount) ®		50	
$R_{\theta JA}$	Junction-to-Ambient		110	

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Static @ T_J = 25°C (unless otherwise specified)

	Parameter	Min.	Тур.	Max.	Units	Conditions
BV_{DSS}	Drain-to-Source Breakdown Voltage	30			V	$V_{GS} = 0V, I_D = 250\mu A$
$\Delta \mathrm{BV}_{\mathrm{DSS}}/\Delta \mathrm{T}_{\mathrm{J}}$	Breakdown Voltage Temp. Coefficient		0.023		V/°C	Reference to 25°C, I _D = 1mA
R _{DS(on)}	Static Drain-to-Source On-Resistance		7.5	9.5	mΩ	V _{GS} = 10V, I _D = 15A ③
			10	12.5		V _{GS} = 4.5V, I _D = 12A ③
$V_{GS(th)}$	Gate Threshold Voltage	1.35	1.80	2.25	V	$V_{DS} = V_{GS}$, $I_D = 250\mu A$
$\Delta V_{GS(th)}/\Delta T_J$	Gate Threshold Voltage Coefficient		-5.0		mV/°C	
I _{DSS}	Drain-to-Source Leakage Current			1.0	μA	$V_{DS} = 24V, V_{GS} = 0V$
				150		$V_{DS} = 24V, V_{GS} = 0V, T_{J} = 125^{\circ}C$
I _{GSS}	Gate-to-Source Forward Leakage			100	nA	V _{GS} = 20V
	Gate-to-Source Reverse Leakage			-100		V _{GS} = -20V
gfs	Forward Transconductance	71			S	V _{DS} = 15V, I _D = 12A
Q_g	Total Gate Charge		9.6	14		
Q_{gs1}	Pre-Vth Gate-to-Source Charge		2.6			V _{DS} = 15V
Q_{gs2}	Post-Vth Gate-to-Source Charge		0.90		nC	V _{GS} = 4.5V
Q_{gd}	Gate-to-Drain Charge		3.5			I _D = 12A
Q_{godr}	Gate Charge Overdrive		2.6			See Fig. 16
Q _{sw}	Switch Charge (Q _{gs2} + Q _{gd})		4.4			
Q _{oss}	Output Charge		5.8		nC	$V_{DS} = 15V, V_{GS} = 0V$
t _{d(on)}	Turn-On Delay Time		8.0			V _{DD} = 16V, V _{GS} = 4.5V ③
t _r	Rise Time		11			I _D = 12A
t _{d(off)}	Turn-Off Delay Time		12		ns	Clamped Inductive Load
t _f	Fall Time		3.3			
C _{iss}	Input Capacitance		1150			$V_{GS} = 0V$
C _{oss}	Output Capacitance		260		pF	V _{DS} = 15V
C _{rss}	Reverse Transfer Capacitance		120			f = 1.0MHz

Avalanche Characteristics

	Parameter	Тур.	Max.	Units
E _{AS}	Single Pulse Avalanche Energy②		42	mJ
I_{AR}	Avalanche Current ①		12	Α
E_{AR}	Repetitive Avalanche Energy ①		5.0	mJ

Diode Characteristics

	Parameter	Min.	Тур.	Max.	Units	Conditions
Is	Continuous Source Current			56④		MOSFET symbol
	(Body Diode)				Α	showing the
I _{SM}	Pulsed Source Current			220		integral reverse
	(Body Diode) ①					p-n junction diode.
V_{SD}	Diode Forward Voltage			1.0	V	$T_J = 25$ °C, $I_S = 12A$, $V_{GS} = 0V$ ③
t _{rr}	Reverse Recovery Time		25	38	ns	$T_J = 25$ °C, $I_F = 12A$, $V_{DD} = 15V$
Q_{rr}	Reverse Recovery Charge		17	26	nC	di/dt = 100A/μs ③
t _{on}	Forward Turn-On Time	Intrinsio	Intrinsic turn-on time is negligible (turn-on is dominated by LS+LD)			



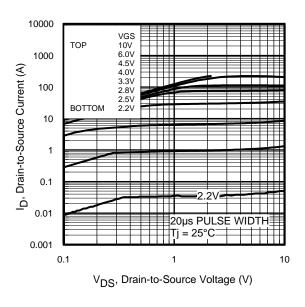


Fig 1. Typical Output Characteristics

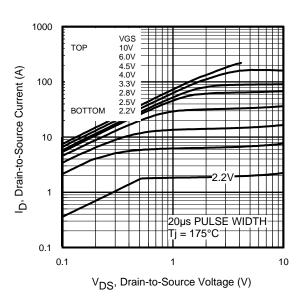


Fig 2. Typical Output Characteristics

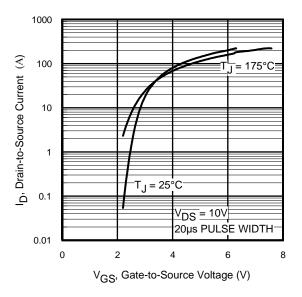


Fig 3. Typical Transfer Characteristics

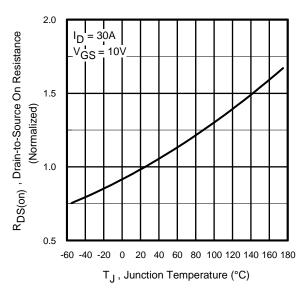


Fig 4. Normalized On-Resistance vs. Temperature



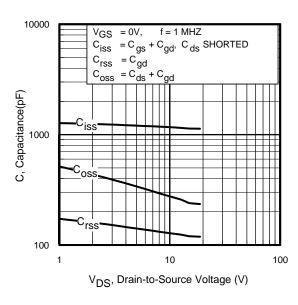


Fig 5. Typical Capacitance vs. Drain-to-Source Voltage

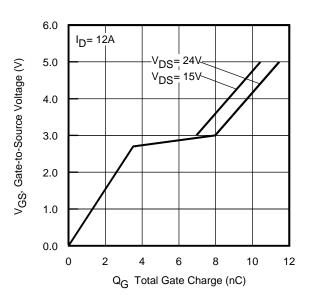


Fig 6. Typical Gate Charge vs. Gate-to-Source Voltage

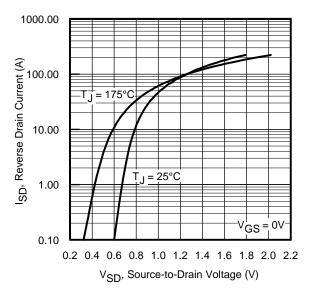


Fig 7. Typical Source-Drain Diode Forward Voltage

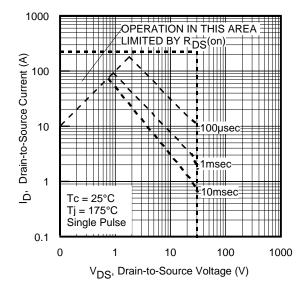
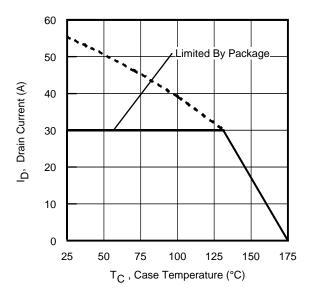


Fig 8. Maximum Safe Operating Area







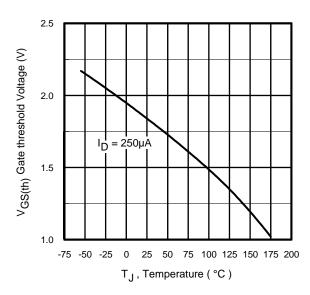


Fig 9. Maximum Drain Current vs. Case Temperature

Fig 10. Threshold Voltage vs. Temperature

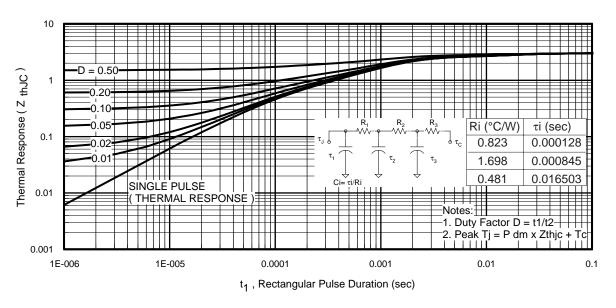


Fig 11. Maximum Effective Transient Thermal Impedance, Junction-to-Case

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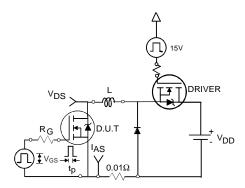


Fig 12a. Unclamped Inductive Test Circuit

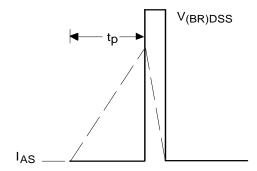


Fig 12b. Unclamped Inductive Waveforms

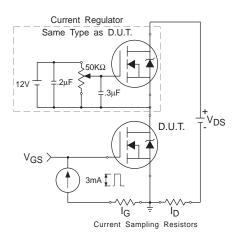


Fig 13. Gate Charge Test Circuit

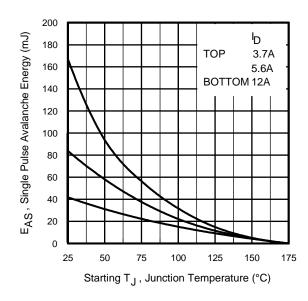


Fig 12c. Maximum Avalanche Energy vs. Drain Current

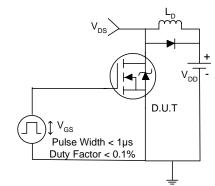


Fig 14a. Switching Time Test Circuit

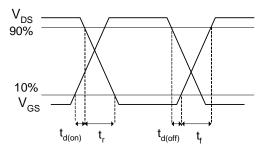


Fig 14b. Switching Time Waveforms



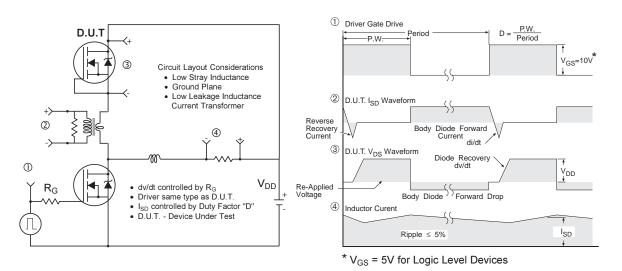


Fig 15. Peak Diode Recovery dv/dt Test Circuit for N-Channel HEXFET® Power MOSFETs

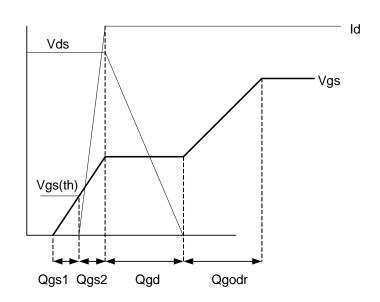


Fig 16. Gate Charge Waveform



Power MOSFET Selection for Non-Isolated DC/DC Converters

Control FET

Special attention has been given to the power losses in the switching elements of the circuit - Q1 and Q2. Power losses in the high side switch Q1, also called the Control FET, are impacted by the $R_{\rm ds(on)}$ of the MOSFET, but these conduction losses are only about one half of the total losses.

Power losses in the control switch Q1 are given by;

$$P_{loss} = P_{conduction} + P_{switching} + P_{drive} + P_{output}$$

This can be expanded and approximated by;

$$\begin{split} P_{loss} &= \left(I_{rms}^{2} \times R_{ds(on)}\right) \\ &+ \left(I \times \frac{Q_{gd}}{i_{g}} \times V_{in} \times f\right) + \left(I \times \frac{Q_{gs2}}{i_{g}} \times V_{in} \times f\right) \\ &+ \left(Q_{g} \times V_{g} \times f\right) \\ &+ \left(\frac{Q_{oss}}{2} \times V_{in} \times f\right) \end{split}$$

This simplified loss equation includes the terms Q_{gs2} and Q_{oss} which are new to Power MOSFET data sheets.

 Q_{gs2} is a sub element of traditional gate-source charge that is included in all MOSFET data sheets. The importance of splitting this gate-source charge into two sub elements, Q_{gs1} and Q_{gs2} , can be seen from Fig 16.

 Q_{gs2} indicates the charge that must be supplied by the gate driver between the time that the threshold voltage has been reached and the time the drain current rises to I_{dmax} at which time the drain voltage begins to change. Minimizing Q_{gs2} is a critical factor in reducing switching losses in Q1.

 $\rm Q_{\rm oss}$ is the charge that must be supplied to the output capacitance of the MOSFET during every switching cycle. Figure A shows how $\rm Q_{\rm oss}$ is formed by the parallel combination of the voltage dependant (nonlinear) capacitance's $\rm C_{\rm ds}$ and $\rm C_{\rm dg}$ when multiplied by the power supply input buss voltage.

Synchronous FET

The power loss equation for Q2 is approximated by:

$$\begin{split} P_{loss} &= P_{conduction} + P_{drive} + P_{output}^* \\ P_{loss} &= \left(I_{rms}^2 \times R_{ds(on)}\right) \\ &+ \left(Q_g \times V_g \times f\right) \\ &+ \left(\frac{Q_{oss}}{2} \times V_{in} \times f\right) + \left(Q_{rr} \times V_{in} \times f\right) \end{split}$$

*dissipated primarily in Q1.

For the synchronous MOSFET Q2, $R_{\text{ds(on)}}$ is an important characteristic; however, once again the importance of gate charge must not be overlooked since it impacts three critical areas. Under light load the MOSFET must still be turned on and off by the control IC so the gate drive losses become much more significant. Secondly, the output charge Q_{oss} and reverse recovery charge Q_{rr} both generate losses that are transfered to Q1 and increase the dissipation in that device. Thirdly, gate charge will impact the MOSFETs' susceptibility to Cdv/dt turn on.

The drain of Q2 is connected to the switching node of the converter and therefore sees transitions between ground and $V_{\rm in}.$ As Q1 turns on and off there is a rate of change of drain voltage dV/dt which is capacitively coupled to the gate of Q2 and can induce a voltage spike on the gate that is sufficient to turn the MOSFET on, resulting in shoot-through current . The ratio of $Q_{\rm gd}/Q_{\rm gs1}$ must be minimized to reduce the potential for Cdv/dt turn on.

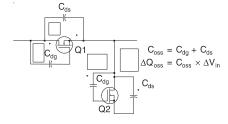
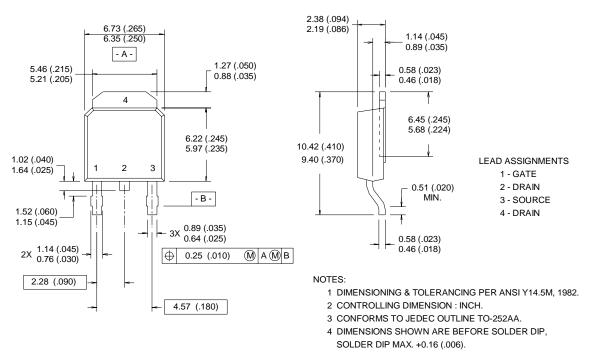


Figure A: Q_{oss} Characteristic



D-Pak (TO-252AA) Package Outline

Dimensions are shown in millimeters (inches)

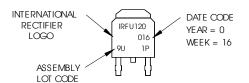


D-Pak (TO-252AA) Part Marking Information

Notes: This part marking information applies to devices produced before 02/26/2001

EXAMPLE: THIS IS AN IRFR120 WITH ASSEMBLY

LOT CODE 9U1P

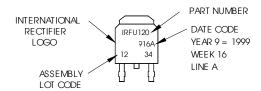


Notes: This part marking information applies to devices produced after 02/26/2001

EXAMPLE: THIS IS AN IRFR120 WITH ASSEMBLY

LOT CODE 1234 ASSEMBLED ON WW 16, 1999

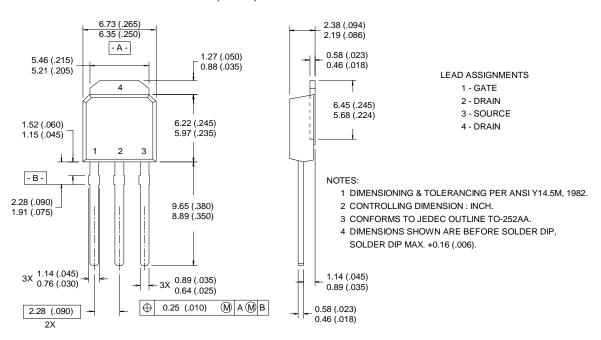
IN THE ASSEMBLY LINE "A"





I-Pak (TO-251AA) Package Outline

Dimensions are shown in millimeters (inches)

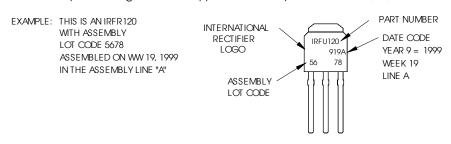


I-Pak (TO-251AA) Part Marking Information

Notes: This part marking information applies to devices produced before 02/26/2001



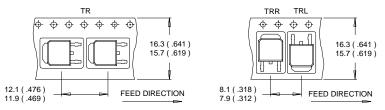
Notes: This part marking information applies to devices produced after 02/26/2001



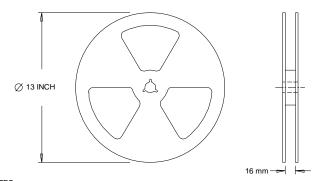


D-Pak (TO-252AA) Tape & Reel Information

Dimensions are shown in millimeters (inches)



- 1. CONTROLLING DIMENSION: MILLIMETER.
 2. ALL DIMENSIONS ARE SHOWN IN MILLIMETERS (INCHES).
 3. OUTLINE CONFORMS TO EIA-481 & EIA-541.



NOTES:
1. OUTLINE CONFORMS TO EIA-481.

Notes:

- ① Repetitive rating; pulse width limited by max. junction temperature.
- Starting $T_J = 25$ °C, L = 0.58mH, $R_G = 25\Omega$, $I_{AS} = 12A$.
- 3 Pulse width \leq 400 μ s; duty cycle \leq 2%.
- 4 Calculated continuous current based on maximum allowable junction temperature. Package limitation current is 30A.
- ⑤ When mounted on 1" square PCB (FR-4 or G-10 Material). For recommended footprint and soldering techniques refer to application note #AN-994.

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