## Overview

The LB1875 is a predriver IC for polygon mirror motors. By using a driver array or discrete transistors (FETs) at the output, motor drive with high rotation precision is possible. PAM drive or direct PWM drive can be selected for the output to realize high-efficiency control with minimum power loss.

## Features

- Three-phase bipolar drive
- Direct PWM drive (bottom side) or PAM drive selectable
- PLL speed control circuit
- PWM oscillator
- Quartz oscillator
- Frequency divider
- FG with Schmitt comparator
- FG input single edge, dual edge selector circuit
- Integrating amplifier
- Phase lock detector output
- Current limiter
- Motor lock protection
- Thermal protection
- Forward/reverse circuit
- 5 V regulator output


## Package Dimensions

unit: mm
3235-HSOP36


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## Specifications

Maximum Ratings at $\mathbf{T a}=25^{\circ} \mathrm{C}$

| Parameter | Symbol | Conditions | Ratings | Unit |
| :--- | :---: | :---: | :---: | :---: |
| Maximum supply voltage | $\mathrm{V}_{\mathrm{CC}} \max$ |  | 14.5 | V |
| Output current | $\mathrm{I}_{0} \max$ |  | 30 | mA |
| Allowable power dissipation | Pd max | IC only | 0.9 | W |
|  |  | with substrate $\left(114.3 \times 76.1 \times 1.6 \mathrm{~mm}^{3}\right.$, <br> glass exposy $)$ | 2.1 | W |
| Operating temperature | Topr |  | -20 to +80 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature | Tstg |  | -55 to +150 | ${ }^{\circ} \mathrm{C}$ |

Operation Conditions at $\mathrm{Ta}=25^{\circ} \mathrm{C}$

| Parameter | Symbol | Conditions | Ratings | Unit |
| :--- | :---: | :---: | ---: | :---: |
| Maximum supply voltage | $\mathrm{V}_{\mathrm{CC}} 1$ |  | 8 to 13.5 | V |
|  | $\mathrm{~V}_{\mathrm{CC}} 2$ | When shorted between $\mathrm{V}_{\mathrm{CC}}$ and $\mathrm{V}_{\text {REG }}$ | 4.5 to 5.5 | V |
| Output current | $\mathrm{I}_{\mathrm{C}}$ |  | 20 | mA |
| 5 V regulated output current | $\mathrm{I}_{\text {REG }}$ |  | 0 to -20 | mA |
| Voltage applied at LD pin | $\mathrm{V}_{\mathrm{LD}}$ |  | 0 to 13.5 | V |
| LD pin output current | $\mathrm{I}_{\mathrm{LD}}$ |  | 0 to 10 | mA |
| Voltage applied at PWM pin | $\mathrm{V}_{\text {PWM }}$ |  | 0 to 13.5 | V |
| PWM pin output current | $\mathrm{I}_{\mathrm{PWM}}$ |  | 0 to 20 | mA |



LB1875

Electrical Characteristics at $\mathbf{T a}=\mathbf{2 5}{ }^{\circ} \mathbf{C}, \mathbf{V}_{\mathrm{CC}}=\mathbf{1 2 V}$

| Parameter | Symbol | Conditions | Ratings |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | min | typ | max |  |
| Power supply current | $\mathrm{I}_{\mathrm{cc}}$ |  |  | 30 | 40 | mA |
| [5V regulated output ] |  |  |  |  |  |  |
| Output fluctuation | $\mathrm{V}_{\text {REG }}$ |  | 4.65 | 5.0 | 5.35 | V |
| Voltage fluctuation | $\Delta \mathrm{V}_{\text {REG }} 1$ | $\mathrm{V}_{\mathrm{cc}}=8$ to 13.5 V |  | 40 | 100 | mV |
| Load fluctuation | $\Delta \mathrm{V}_{\text {REG }} 2$ | $\mathrm{lo}=0$ to -15 mA |  | 20 | 100 | mV |
| Temperature coefficcient | $\Delta \mathrm{V}_{\text {REG }} 3$ | Design target value |  | 0 |  | $\mathrm{mV} /{ }^{\circ} \mathrm{C}$ |
| [Output Section] |  |  |  |  |  |  |
| Output saturation voltage | $\mathrm{V}_{\text {O }}$ (sat)1-1 | UH, VH, WH "L" level, $\mathrm{l}_{0}=50 \mu \mathrm{~A}$ |  | 0.1 | 0.3 | V |
|  | Vo(sat)1-2 | UH, VH, WH "L" level, $\mathrm{l}_{0}=10 \mathrm{~mA}$ |  | 0.9 | 1.1 | V |
|  | $\mathrm{V}_{\text {( }}$ (sat)2 | UH, VH, WH "L" level, $\mathrm{l}_{0}=20 \mathrm{~mA}$ |  | $\mathrm{V}_{\mathrm{cc}}-0.9$ | $\mathrm{V}_{\mathrm{cc}}-1.1$ | V |
|  | $\mathrm{V}_{\text {o }}$ (sat) 3 | UL, VL, WL, $\mathrm{l}=20 \mathrm{~mA}$ |  | 0.2 | 0.4 | V |
| Output leak current | Ioleak | UL, VL, WL |  |  | 10 | $\mu \mathrm{A}$ |
| [Hall amplifier] |  |  |  |  |  |  |
| Input bias current | $\mathrm{I}_{\text {нв }}(\mathrm{HA})$ |  | -4 | -1 |  | $\mu \mathrm{A}$ |
| Same-phase input voltage range | $\mathrm{V}_{\text {ICM }}$ |  | 0 |  | $\mathrm{V}_{\mathrm{cc}}-2.0$ | V |
| Hall input sensitivity |  |  | 30 |  |  | $m V_{\text {p.p }}$ |
| Hysteresis width | $\Delta \mathrm{V}_{\text {IN }}(\mathrm{HA})$ |  | 8 | 14 | 24 | mV |
| Input voltage L->H | $\mathrm{V}_{\text {SLH }}$ |  |  | 7 |  | mV |
| Input voltage $\mathrm{H}->\mathrm{L}$ | $\mathrm{V}_{\text {SHL }}$ |  |  | -7 |  | mV |
| [FG/Schmitt comparator section] |  |  |  |  |  |  |
| Input bias current | $\mathrm{I}_{\mathrm{B}}$ (FGS) |  | -4 | -1 |  | $\mu \mathrm{A}$ |
| Same-phase input voltage range | $\mathrm{V}_{\text {ICM }}(\mathrm{FGS})$ |  | 0 |  | $\mathrm{V}_{\mathrm{cc}}-2.0$ | V |
| Input sensitivity | $\mathrm{V}_{10}(F G S)$ |  | 30 |  |  | $m V_{\text {p.p }}$ |
| Hysteresis width | $\Delta \mathrm{V}_{\mathbb{N}}(\mathrm{FGS})$ | Design target value | 8 | 14 | 24 | mV |
| Input voltage L->H | $\mathrm{V}_{\text {SLH }}(\mathrm{FGS})$ | Design target value |  | 7 |  | mV |
| Input voltage $\mathrm{H}->\mathrm{L}$ | $\mathrm{V}_{\text {SHL }}(\mathrm{FGS})$ | Design target value |  | -7 |  | mV |
| [PWM oscillator] |  |  |  |  |  |  |
| Output High level voltage | $\mathrm{V}_{\text {он }}(\mathrm{OSC})$ |  | 2.7 | 3.0 | 3.3 | V |
| Output Low level voltage | $\mathrm{V}_{\text {OL }}(\mathrm{OSC})$ |  | 1.5 | 1.8 | 2.1 | V |
| Oscillator frequency | f(OSC) | $\mathrm{C}=2200 \mathrm{pF}$ |  | 30 |  | kHz |
| Amplitude | V(OSC) |  | 1.0 | 1.2 | 1.4 | $\mathrm{V}_{\text {P.p }}$ |
| [PWM output] |  |  |  |  |  |  |
| Output saturation voltage | $\mathrm{V}_{\text {o( }}(\mathrm{PWM})$ | $\mathrm{l}_{\text {pwn }}=15 \mathrm{~mA}$ |  | 0.9 | 2.0 | V |
| Output leak current | IL(PWM) | $\mathrm{V}_{\mathrm{o}}=\mathrm{V}_{\text {cc }}$ |  |  | 10 | $\mu \mathrm{A}$ |
| [CSD oscillator ] |  |  |  |  |  |  |
| Output High level voltage | $\mathrm{V}_{\text {OH }}$ (CSD) |  | 2.5 | 2.8 | 3.1 | V |
| Output Low level voltage | $V_{\text {oı( }}$ (CSD) |  | 0.55 | 0.85 | 1.15 | V |
| External C charge current | $\mathrm{I}_{\mathrm{CHG} 1} 1$ |  | -13 | -10 | -7 | $\mu \mathrm{A}$ |
| External C discharge current | $\mathrm{I}_{\mathrm{CHG}} 2$ |  | 7 | 10 | 13 | $\mu \mathrm{A}$ |
| Oscillator frequency | $\mathrm{f}_{\text {cso }}$ | $\mathrm{C}=0.068 \mu \mathrm{~F}$ |  | 35 |  | Hz |
| Amplitude | $\mathrm{V}_{\text {csD }}$ |  | 1.75 | 1.95 | 2.15 | $\mathrm{V}_{\mathrm{p} \text { - }}$ |
| [Phase comparator output] |  |  |  |  |  |  |
| Output High level voltage | $\mathrm{V}_{\text {PDH }}$ | $\mathrm{I}_{\text {OH }}=-100 \mu \mathrm{~A}$ | $V_{\text {REG }}-0.2$ | $\mathrm{V}_{\text {REG }}-0.1$ |  | V |
| Output Low level voltage | $\mathrm{V}_{\text {PDL }}$ | $\mathrm{l}_{\mathrm{OH}}=100 \mu \mathrm{~A}$ |  | 0.1 | 0.2 | V |
| Output source current | $\mathrm{IPD}^{+}$ | $\mathrm{V}_{\text {PD }}=\mathrm{V}_{\text {REG }} / 2$ |  |  | -0.6 | mA |
| Output sink current | $\mathrm{IPD}^{-}$ | $\mathrm{V}_{\text {PD }}=\mathrm{V}_{\text {REG }} / 2$ | 1.5 |  |  | mA |
| [Phase lock detector output] |  |  |  |  |  |  |
| Output saturation voltage | $\mathrm{V}_{\text {oL }}(\mathrm{LD})$ | l Lo $=10 \mathrm{~mA}$ |  | 0.1 | 0.4 | V |
| Output leak current | $I_{\text {L }}($ LD $)$ | $\mathrm{V}_{\mathrm{o}}=\mathrm{V}_{\text {cc }}$ |  |  | 10 | $\mu \mathrm{A}$ |

LB1875
Continued from preceding page

| Parameter | Symbol | Conditions | Ratings |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | min | typ | max |  |
| [ERR amplifier] |  |  |  |  |  |  |
| Input offset voltage | $\mathrm{V}_{10}$ (ER) | Design target value | -10 |  | +10 | mV |
| Input bias current | $\mathrm{I}_{\mathrm{B}}(\mathrm{ER})$ |  | -1 |  | +1 | $\mu \mathrm{A}$ |
| Ouput High level voltage | $\mathrm{V}_{\text {OH }}(\mathrm{ER})$ | $\mathrm{I}_{\mathrm{OH}}=-500 \mu \mathrm{~A}$ | $\mathrm{V}_{\text {REG }}-1.2$ | $\mathrm{V}_{\text {REG }}-0.9$ |  | V |
| Ouput Low level voltage | $\mathrm{V}_{\text {oL }}(E R)$ | $\mathrm{l}_{\mathrm{o}}=500 \mu \mathrm{~A}$ |  | 0.9 | 1.2 | V |
| DC bias level | $\mathrm{V}_{\mathrm{B}}$ (ER) |  | -5\% | $\mathrm{V}_{\text {REG }} / 2$ | + 5\% | V |
| [Current limiter] |  |  |  |  |  |  |
| Limiter voltage | $\mathrm{V}_{\text {RF }}$ |  | 0.45 | 0.5 | 0.55 | V |
| [Low-voltage protection circuit] |  |  |  |  |  |  |
| Operation voltage | $\mathrm{V}_{\text {SoL }}$ |  | 3.55 | 3.75 | 3.95 | V |
| Release voltage | $\mathrm{V}_{\text {SOH }}$ |  | 3.8 | 4.0 | 4.2 | V |
| Hysteresis width | $\Delta \mathrm{VSD}$ |  | 0.15 | 0.25 | 0.35 | ${ }^{\circ} \mathrm{C}$ |
| [Thermal shutdown operation] |  |  |  |  |  |  |
| Termal shutdown temperature | TSD | Design target value (junction temperature) | 150 | 180 |  | ${ }^{\circ} \mathrm{C}$ |
| Hysteresis width | $\Delta T S D$ | Design target value (junction temperature) |  | 30 |  | ${ }^{\circ} \mathrm{C}$ |
| [SOFT pin] |  |  |  |  |  |  |
| Stop voltage | $\mathrm{V}_{\text {SFT }}$ | In stop condition | 3.0 | 3.3 | 3.6 | V |
| External C discharge current | $\mathrm{I}_{\text {DCHG }}$ |  | 4 | 6 | 8 | $\mu \mathrm{A}$ |
| [Quartz oscillator] |  |  |  |  |  |  |
| Quartz oscillator frequency | fosc |  | 2 |  | 10 | MHz |
| Low level pin voltage | $\mathrm{V}_{\text {oscl }}$ | $\mathrm{losc}=-0.5 \mathrm{~mA}$ |  | 1.45 |  | V |
| High level pin voltage | $\mathrm{V}_{\text {OSCH }}$ | $\mathrm{V}_{\text {osc }}=\mathrm{V}_{\text {oscl }}+0.6 \mathrm{~V}$ |  | 0.5 |  | mA |
| [CLK ${ }_{\text {out }}$ pin] |  |  |  |  |  |  |
| Output saturation voltage | $\mathrm{V}_{\text {ol(CKOUT) }}$ | $\mathrm{I}_{\text {ckout }}=2 \mathrm{~mA}$ |  | 0.1 | 0.4 | V |
| Output leak current | IL(CKOUT) | $\mathrm{V}_{\mathrm{o}}=\mathrm{V}_{\mathrm{cc}}$ |  |  | 10 | $\mu \mathrm{A}$ |
| [CLK ${ }_{\text {IN }}$ pin] |  |  |  |  |  |  |
| External input frequency | $\mathrm{f}_{\text {(CKIN) }}$ |  | 0.1 |  | 10 | kHz |
| High level input voltage | $\mathrm{V}_{\mathbf{H H}(\mathrm{CKIN})}$ |  | 3.5 |  | $\mathrm{V}_{\text {REG }}$ | V |
| Low level input voltage | $\mathrm{V}_{\text {LICKİ }}$ ) |  | 0 |  | 1.5 | V |
| Input open voltage | $\mathrm{V}_{10 \text { (CKIN) }}$ |  | $\mathrm{V}_{\text {REG }}-0.5$ |  | $\mathrm{V}_{\text {REG }}$ | V |
| Hysteresis width | $\mathrm{V}_{\text {ISICKIN) }}$ |  | 0.3 | 0.4 | 0.5 | V |
| High level input current | $\mathrm{I}_{\mathrm{HI}(\mathrm{CKIN})}$ | $\mathrm{V}_{\text {CKIN }}=\mathrm{V}_{\text {REG }}$ | -10 | 0 | +10 | $\mu \mathrm{A}$ |
| Low level input current | $\mathrm{I}_{\text {L(CKIN) }}$ | $\mathrm{V}_{\text {CKIN }}=0 \mathrm{~V}$ | -200 | -140 |  | $\mu \mathrm{A}$ |
| [S/S pin] |  |  |  |  |  |  |
| High level input voltage | $\mathrm{V}_{\mathrm{H}}(\mathrm{SS})$ |  | 3.5 |  | $\mathrm{V}_{\text {REG }}$ | V |
| Low level input voltage | $\mathrm{V}_{\text {LL }}(\mathrm{SS}$ ) |  | 0 |  | 1.5 | V |
| Input open voltage | $\mathrm{V}_{10}(\mathrm{SS})$ |  | $\mathrm{V}_{\text {REG }}-0.5$ |  | $\mathrm{V}_{\text {REG }}$ | V |
| Hysteresis width | $\mathrm{V}_{\text {IS }}(\mathrm{SS})$ |  | 0.3 | 0.4 | 0.5 | V |
| High level input current | $\mathrm{I}_{\mathrm{H}}(\mathrm{SS})$ | $\mathrm{VS} / \mathrm{S}=\mathrm{V}_{\text {REG }}$ | -10 | 0 | +10 | $\mu \mathrm{A}$ |
| Low level input current | $1 / 2(S S)$ | VS/S=0V | -200 | -140 |  | $\mu \mathrm{A}$ |
| [F/R pin] |  |  |  |  |  |  |
| High level input voltage | $\mathrm{V}_{\mathbf{H}}(\mathrm{FR})$ |  | 3.5 |  | $\mathrm{V}_{\text {REG }}$ | V |
| Low level input voltage | $\mathrm{V}_{\mathrm{LL}}(\mathrm{FR})$ |  | 0 |  | 1.5 | V |
| Input open voltage | $\mathrm{V}_{10}(\mathrm{FR})$ |  | $\mathrm{V}_{\text {REG }}-0.5$ |  | $\mathrm{V}_{\text {REG }}$ | V |
| High level input current | $\mathrm{I}_{\mathbf{H}}(\mathrm{FR})$ | $\mathrm{VF} / \mathrm{R}=\mathrm{V}_{\text {REG }}$ | -10 | 0 | +10 | $\mu \mathrm{A}$ |
| Low level input current | $\mathrm{I}_{1}(\mathrm{FR})$ | $\mathrm{VF} / \mathrm{R}=0 \mathrm{~V}$ | -200 | -140 |  | $\mu \mathrm{A}$ |
| [FG $\left.{ }_{\text {sel }} \mathrm{pin}\right]$ |  |  |  |  |  |  |
| High level input voltage | $\mathrm{V}_{\text {HH }}(\mathrm{FSEL})$ |  | 3.5 |  | $\mathrm{V}_{\text {REG }}$ | V |
| Low level input voltage | $\mathrm{V}_{12}$ (FSEL) |  | 0 |  | 1.5 | V |
| Input open voltage | $\mathrm{V}_{10}($ FSEL $)$ |  | $\mathrm{V}_{\text {REG }}-0.5$ |  | $\mathrm{V}_{\text {REG }}$ | V |
| High level input current | $\mathrm{I}_{\mathrm{H}}($ FSEL) | $V_{\text {FSEL }}=V_{\text {REG }}$ | -10 | 0 | +10 | $\mu \mathrm{A}$ |
| Low level input current | $1 \mathrm{I}_{\text {L }}(\mathrm{FSEL})$ | $\mathrm{V}_{\text {FSEL }}=0 \mathrm{~V}$ | -200 | -140 |  | $\mu \mathrm{A}$ |

LB1875
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| Parameter | Symbol | Conditions | Ratings |  |  | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | min | typ | max |  |
| [CLK ${ }_{\text {sEL }}$ pin] |  |  |  |  |  |  |
| High level input voltage | $\mathrm{V}_{1 H}(\mathrm{CSEL})$ |  | 4.0 |  | $\mathrm{V}_{\text {REG }}$ | V |
| Middle level input voltage | $\mathrm{V}_{\text {IM }}(\mathrm{CSEL})$ |  | 2.0 |  | 3.0 | V |
| Low level input voltage | $\mathrm{V}_{\mathrm{IL}}$ (CSEL) |  | 0 |  | 1.0 | V |
| Input open voltage | $\mathrm{V}_{10}(\mathrm{CSEL})$ |  | $\mathrm{V}_{\text {REG }}-0.5$ |  | $\mathrm{V}_{\text {REG }}$ | V |
| High level input current | $\mathrm{I}_{1+}(\mathrm{CSEL})$ | $\mathrm{V}_{\text {CSEL }}=\mathrm{V}_{\text {REG }}$ | -10 | 0 | +10 | $\mu \mathrm{A}$ |
| Low level input current | $\mathrm{I}_{1}(\mathrm{CSEL})$ | $\mathrm{V}_{\text {CSEL }}=0 \mathrm{~V}$ | -200 | -140 |  | $\mu \mathrm{A}$ |
| [LIM pin] |  |  |  |  |  |  |
| High level input voltage | $\mathrm{V}_{\text {IH }}$ (LIM) |  | 3.5 |  | $\mathrm{V}_{\text {REG }}$ | V |
| Low level input voltage | $\mathrm{V}_{\text {IL }}$ (LIM) |  | 0 |  | 1.5 | V |
| Input open voltage | $\mathrm{V}_{10}$ (LIM) |  | $\mathrm{V}_{\text {REG }}=0.5$ |  | $\mathrm{V}_{\text {REG }}$ | V |
| High level input current | $\mathrm{I}_{\mathrm{HH}}($ LIM $)$ | $\mathrm{V}_{\text {LIM }}=\mathrm{V}_{\text {REG }}$ | -10 | 0 | +10 | $\mu \mathrm{A}$ |
| Low level input current | $\mathrm{I}_{1 L}(\mathrm{LIM})$ | $\mathrm{V}_{\text {LIM }}=0 \mathrm{~V}$ | -200 | -140 |  | $\mu \mathrm{A}$ |

3-phase logic truth table ( $\mathbf{I N}=$ " H " indicates the $\mathrm{IN}^{+}>\mathrm{IN}^{-}$condition)

|  | F/R="L" |  |  | F/R="H" |  |  | Output |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | IN1 | IN2 | IN3 | IN1 | IN2 | IN3 | SOURCE | SYNC |
| 1 | H | L | H | L | H | L | VH | UL |
| 2 | H | L | L | L | H | H | WH | UL |
| 3 | H | H | L | L | L | H | WH | VL |
| 4 | L | H | L | H | L | H | UH | VL |
| 5 | L | H | H | H | L | L | UH | WL |
| 6 | L | L | H | H | H | L | VH | WL |

S/S pin

| Input state | Condition |
| :---: | :---: |
| High or open | Stop |
| L | Start |

FGSEL pin

| Input state | Edge detection |
| :---: | :---: |
| High or open | FG dual edge |
| L | FG single edge |

CLKSEL pin

| Input state | Divisor |
| :---: | :---: |
| High or open | $1024 \times 4$ |
| M | 1024 |
| L | $1024 \times 3$ |

## LIM pin

| Input state | Output pin (UH, VH, WH) | PWMOUT pin |
| :---: | :---: | :---: |
| High or open | No PWM (PAM operation) | PWM output |
| L | PWM (direct PWN operation) | FG/Schmitt comparator output |

Pin Assignment


## Block Diagram and Sample Application Circuit

 (Sample application: PAM drive, FET output)

Note: For applications where the motor has variable speed and control at low motor voltages is required, the base voltage of the output interface transistor must be made low. In this case, a P-channel FET which can be used at low gate voltages must be selected.
(Sample application: direct PWM drive, FET output)

(Sample application: PAM drive, bipolar transistor output)


## Description of the LB1875

## 1. Speed control circuit

This IC uses the PLL speed control technique which allows stable, high-precision motor rotation with low jitter. The PLL circuit performs phase comparison of the falling edge of the clock input $\left(\mathrm{CLK}_{\mathrm{IN}}\right)$ with the edge of the FG input. Control is based on the differential output.
When the $\mathrm{FG}_{\text {SEL }}$ pin is Low, only the falling edge of the FG signal is valid. When the pin is High or open, both edges are valid. When both edges are used, the FG waveform precision becomes critical.
When using an external clock input (supplied from CLK $_{\text {IN }}$ pin), the FG servo frequency is determined by the following equation.
$\mathrm{f}_{\mathrm{FG}}($ servo $)=\mathrm{f}_{\mathrm{CLK}} \quad\left(\mathrm{FG}_{\mathrm{SEL}}=\right.$ Low $)$
$\mathrm{f}_{\mathrm{FG}}($ servo $)=\mathrm{f}_{\mathrm{CLK}} / 2 \quad\left(\mathrm{FG}_{\mathrm{SEL}}=\right.$ High or open $)$
When using the internal clock, the FG servo frequency is determined by the following equation. The number of FG pulses and the quartz oscillator frequency determine the motor rotation speed.
$\mathrm{f}_{\mathrm{FG}}($ servo $)=\mathrm{f}_{\mathrm{OSC}} / \mathrm{N} \quad\left(\mathrm{FG}_{\mathrm{SEL}}=\right.$ Low $)$
$\mathrm{f}_{\mathrm{FG}}($ servo $)=\mathrm{f}_{\mathrm{OSC}} / 2 \mathrm{~N} \quad\left(\mathrm{FG}_{\mathrm{SEL}}=\right.$ High or open $)$
$\mathrm{f}_{\text {OSC }}$ : Quartz oscillator frequency
N : Clock divisor (see table)

## 2. Output drive

This IC allows selection of PAM drive or direct PWM drive.
When the LIM pin is Low, the direct PWM mode is selected. The ON duty cycle of the UH, VH, and WH output (external bottomside transistor drive output) changes, thereby controlling the motor speed. Current control is also realized by changing the ON duty cycle to limit the current. At this time, the Schmitt comparator output of the FG is supplied at the PWM ${ }_{\text {out }}$ pin. When bipolar transistors are used externally, the top-side transistors should not have an integrated diode, but Schottky barrier diodes should be used instead (to prevent feedthrough current caused by diode reverse recovery during PWM switching).
When the LIM pin is High or open, the PAM drive mode is selected. The $\mathrm{PWM}_{\text {out }}$ pin carries the PWM signal. This output can drive an external switching regulator circuit for varying the motor supply voltage and thereby controlling motor speed. Current control is also realized by changing the motor supply voltage. In this case, a delay in the switching regulator circuit will cause a delay in the current control action. During the delay, a higher current than the set current may flow, which must be taken into consideration when selecting output transistors. For applications where the motor has variable speed and control at low motor voltages is required, the lowest operation voltage is limited by the base voltage of the interface transistor for top-side output transistor drive. If this causes a problem, the base voltage must be made low (for example by dividing the $\mathrm{V}_{\text {REG }}$ voltage with resistors). When FETs are used as topside output transistors, types which can be used at low gate voltages must be selected.

## 3. Current limiting circuit

The current limiting circuit limits the peak current to the value $\mathrm{I}=\mathrm{V}_{\mathrm{RF}} / \mathrm{Rf}\left(\mathrm{V}_{\mathrm{RF}}=0.5 \mathrm{~V}\right.$ typ., Rf: current detector resistor). As mentioned above, in PAM drive mode, a current higher than the set current may flow during the delay interval. If the capacitor charge current of the switching regulator circuit is a problem, a smoothing capacitor may be inserted, with the negative side connected to the RF pin.
If PWM noise is a problem in the RF waveform, a filter should be provided at the input.

## 4. Reference clock

Since the clock input of the PLL circuit $\left(\mathrm{CLK}_{\mathrm{IN}}\right)$ and the internal divisor output ( $\mathrm{CLK}_{\mathrm{oUT}}$ ) are separate, various applications are possible.
(1) Using the internal divider circuit

Basically, $\mathrm{CLK}_{\mathrm{IN}}$ and $\mathrm{CLK}_{\text {out }}$ are shorted. If a division ratio other than the built-in ratio is required, an external divider circuit can be inserted between these two pins.
[1] Using a quartz oscillator
An oscillator using a quartz crystal and $\mathrm{C}, \mathrm{R}$ components can be configured as shown below.


## C1, R1 : For stable oscillation <br> C2 : For overtone oscillation prevention <br> C3 : For crystal coupling

(Reference values)

| Oscillator frequency $(\mathrm{MHz})$ | $\mathrm{C} 1(\mu \mathrm{~F})$ | $\mathrm{C} 2(\mathrm{pF})$ | $\mathrm{C} 3(\mathrm{pF})$ | $\mathrm{R} 1(\Omega)$ |
| :---: | :---: | :---: | :---: | :---: |
| 2 to 3 | 0.1 | 10 | 100 | 330 k |
| 3 to 7 | 0.1 | None | 47 | 330 k |
| 7 to 9 | 0.1 | None | 22 | 330 k |
| 9 to 10 | 0.1 | None | 12 | 330 k |

The circuit configuration and values are for reference only. The quartz crystal characteristics as well as the possibility of floating capacitance and noise due to layout factors must be taken into consideration when designing an actual application.
[Precautions for wiring layout design]
Since the quartz oscillator circuit operates at high frequencies, it is susceptible to the influence of floating capacitance from the circuit board. Wiring should be kept as short as possible and traces should be kept narrow.
[2] External clock input (equivalent to quartz oscillator, several MHz)
When using an external signal source instead of a quartz oscillator, a resistor of about $13 \mathrm{k} \Omega$ should be inserted in series at the XI input. The XO pin should be left open.
Signal input level
Low: 0 to 0.8 V
High: 2.5 to 5 V
(2) When not using the internal divider circuit

When using an external signal source to supply a signal equivalent to the FG frequency (several kHz ), the signal is input via the $\mathrm{CLK}_{\text {IN }}$ pin. When not using a quartz oscillator, the $\mathrm{X}_{\mathrm{I}}$ pin should be left open or connected to the $\mathrm{V}_{\text {REG }}$ pin (XO is open).

## 5. Hall input signal

The Hall input requires a signal with an amplitude of at least the hysteresis width ( 24 mV max.). Taking possible noise influences into consideration, an amplitude of at least 100 mV is desirable. If noise at the Hall input is a problem, a noise-canceling capacitor (about 0.001 to $0.1 \mu \mathrm{~F}$ ) should be connected across the Hall input pins .
Since the same-phase input range is 0 to $\mathrm{V}_{\mathrm{CC}}-2 \mathrm{~V}$, a Hall element can be connected in series if 12 V is applied at the $\mathrm{V}_{\mathrm{CC}}$ pin.

## 6. FG input signal

The FG input is designed mainly for input from a Hall element and has the same specifications as the Hall input. If the input is to be used for an FG pattern or other very low-level signal, an external amplifier must be used to amplify the signal first.
When there is noise at the FG input, locking may be impaired and jitter may increase. If PWM switching noise or other noise is found to be present, countermeasures such as making the Hall element power supply more stable or connecting a capacitor across the input will be necessary.

## 7. PWM frequency

The PWM frequency is determined by the capacitance connected to the $\mathrm{C}_{\mathrm{PWM}}$ pin.
f PWM $\fallingdotseq 1 /(15000 \times \mathrm{C})$
The PWM frequency should be between 15 and 50 kHz . If the frequency is too low, noise and control performance may be a problem. If it is too high, switching losses will increase.

## 8. LD output

The LD1 output is ON when phase lock is achieved. Phase lock is evaluated only by the phase (through edge comparison), not by speed deviation. Therefore when LD1 is ON, speed deviation is affected by the FG signal acceleration for example when establishing the lock condition. (The lower the acceleration, the lower the speed deviation.) When it is necessary to limit speed deviation when LD1 is ON, the results of actual motor speed measurement must be applied.

## 9. Power supply

When using FETs as bottom-side output transistors, applying a voltage of 12 V to the $\mathrm{V}_{\mathrm{CC}}$ pin makes it possible to supply a gate voltage of about 10 V . When using FETs or bipolar transistors that can handle a low gate voltage, the $\mathrm{V}_{\mathrm{CC}}$ and $\mathrm{V}_{\mathrm{REG}}$ pins can also be short- circuited to apply 5 V . (In this case, do not apply voltage higher than 5.5 V .)
Since this IC is designed for use in high-current motors, the power supply line may fluctuate easily. Therefore a capacitor of sufficient capacitance must be provided between the $\mathrm{V}_{\mathrm{CC}}$ pin and ground, to assure stable operation. If a diode is used in the power line for reverse-connection protection, power line fluctuations may be further increased, which will require more capacitance.

## 10. Motor lock protection circuit

To protect the IC and the motor itself when rotation is inhibited, a motor lock protection circuit is provided. If the LD output is High (unlocked) for a certain interval in the start condition, the external bottom-side transistors are turned off. The length of the interval is determined by the capacitance at the CSD pin. A capacitance of $0.1 \mu \mathrm{~F}$ results in a trigger interval of about 10 seconds.
Trigger interval $(S) \fallingdotseq 110 \times \mathrm{C}(\mu \mathrm{F})$
The trigger interval should be set so as to leave sufficient leeway for motor startup. Speed reduction due to clock frequency switching does not trigger the protection circuit.
When the protection circuit has been triggered, the condition can only be canceled by setting the system to the stop condition or by turning the power off and on again. When wishing not to use the motor lock protection circuit, connect the CSD pin to ground.

## 11. Low voltage protection circuit

The low voltage protection circuit cuts off the bottom-side output transistors (external) when the voltage at the $\mathrm{V}_{\mathrm{REG}}$ pin falls below 3.75 V (typ.). The circuit action is released when the voltage rises above approx. 4.0 V (typ.).

## 12. F/R switching

Forward/reverse switching in principle should be carried out while the motor is stopped. If switching is carried out while the motor is running, feedthrough current (due to output transistor delay) is prevented by the circuit design, but a high current will flow in the output transistors (due to counterelectromotive voltage and coil resistance). If such a condition is anticipated, the output transistors must be selected appropriately, to allow handling even higher current than in normal use.

## 13. Soft start

In PAM drive mode, connecting a capacitor (approx. 0.01 to $0.1 \mu \mathrm{~F}$ ) between the SOFT pin and ground enables soft start (gradual increase in PWM ON duty cycle, causing a sloped rise in motor supply voltage). This prevents the current flow exceeding the set current due to switching regulator circuit delay at startup. The Soft start function is active only immediately after motor startup. When the motor is stopped, the output transistors are turned off, therefore the charge accumulated in the switching regulator smoothing capacitors can only be discharged as leak current of the output transistors. When the motor is restarted before the supply voltage has dropped, the soft start function will not be active. Therefore it is necessary to discharge the capacitors via a resistor so that the soft start function operates properly.

Pin Descriptions
Pin number

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LB1875

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Pin number

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| Pin number | Pin name | Equivalent circuit | Pin function |
| :---: | :---: | :---: | :---: |
| 11 | LD1 |  | Phase lock detector output <br> On when PLL phase lock is achieved. <br> Open collector output |
| 12 | LD2 |  | Phase lock detector output <br> (LD1 inverted output) <br> On when PLL phase lock is achieved. <br> Open collector output |
| 13 | PD |  | Phase comparator output (PLL output) Outputs the phase difference as a signal with changing pulse duty cycle. The higher the duty cycle, the higher the output current. |
| 14 | $\mathrm{E}_{1}$ |  | Differential amplifier input |
| 15 | $\mathrm{E}_{0}$ |  | Differential amplifier output <br> Output current increases at Low. |
| 16 | TOC |  | Torque control input <br> Normally connected to EO pin. When TOC pin goes Low, duty cycle of UH, VH, WH (direct PWM mode) or PWM output (PAM mode) changes, resulting in increased torque. |
| 17 | SOFT |  | Soft start control pin <br> Connect to ground via a capacitor. <br> Leave open when soft start is not to be used. |

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| Pin number | Pin name | Equivalent circuit | Pin function |
| :---: | :---: | :---: | :---: |
| 18 | PWM |  | PWM oscillator pin Connect to ground with a capacitor to set oscillation frequency. |
| 19 | PWM ${ }_{\text {out }}$ |  | PWM output <br> Open collector output (Darlington connection). In direct PWM mode (LIM pin Low) the output is an FG Schmitt output. |
| 20 | RF |  | Output current detector pin <br> Connect to ground via a lower resistor. <br> Sets maximum output current $\mathrm{I}_{\text {oUT }}=$ 0.5/Rf. |
| $\begin{aligned} & 21 \\ & 23 \\ & 25 \end{aligned}$ | WH <br> VH <br> UH |  | Output pin (for external bottom-side transistor drive) <br> Performs duty cycle control in direct PWM mode (LIM pin Low). |
| $\begin{aligned} & 22 \\ & 24 \\ & 26 \end{aligned}$ | WL <br> VL <br> UL |  | Output pin (for external bottom-side transistor drive). <br> Open collector output. |

LB1875

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| Pin number | Pin name | Equivalent circuit | Pin function |
| :---: | :---: | :---: | :---: |
| 27 | $\mathrm{V}_{\text {cc }}$ |  | Power supply pin (output and regulator circuit power supply). Connect to ground via capacitor to prevent noise. When using the IC with a single 5 V source, short this pin to the $V_{\text {REG }}$ pin. |
| $\begin{aligned} & 33 \\ & 32 \\ & 31 \\ & 30 \\ & 29 \\ & 28 \end{aligned}$ | $\mathrm{IN} 1^{+}$ <br> IN1- <br> IN2 ${ }^{+}$ <br> $\mathrm{IN} 2^{-}$ <br> IN3 ${ }^{+}$ <br> IN3- |  | Hall inputs for various phases <br> Logic "High" indicates ViN ${ }^{+}>$Vin. |
| $\begin{aligned} & 35 \\ & 34 \end{aligned}$ | $\begin{aligned} & \mathrm{FG}_{\mathbb{I N}^{+}} \\ & \mathrm{FG}_{\mathbb{N}^{-}} \end{aligned}$ |  | FG comparator input <br> Pin 35: Non-inverted input <br> Pin 36: Inverted input |
| 36 | CSD |  | Reference signal oscillator for motor lock protection circuit, clock interruption error protection circuit etc. <br> Connect to ground via capacitor. <br> Connect directly to ground if protection circuit is not to be used. |
| FRAME | GND |  | Ground |

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