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DESCRIPTION

The SC1408 is a low voltage boost controller that operates from a 1.8V to 16.5V input range. A shutdown pin allows the user to turn the controller off reducing supply current to less than 2μ A typical. Output voltage can be preset to 5V or is adjustable from 3V to 16.5V with a resistor divider. The controller changes frequency in low load conditions to improve efficiency.

The SC1408 was designed for two cell Alkaline or single cell Lithium Ion battery applications. With the proper external components it can be used as a boost converter or a buck/boost converter.

A current sense is implemented with an external resistor that is not in the load current path.

The SC1408 operates in "bootstrapped" mode. When the input voltage to the device is less than 2.5V during startup, a low voltage 50% fixed duty cycle oscillator is switched in to initiate boost action.

FEATURES

- 1.8V to 16.5V input range
- Up to 10W output power
- Preset 5V or adjustable output
- Up to 300kHz switching frequency
- 10µA max shutdown current
- Industrial temperature range
- SO-8 or MSOP-8 package

APPLICATIONS

- PDA Power supplies
- Battery powered applications
- Positive LCD Bias generator
- Portable communications (cellular phones)
- Peripheral card supplies
- Industrial power supplies

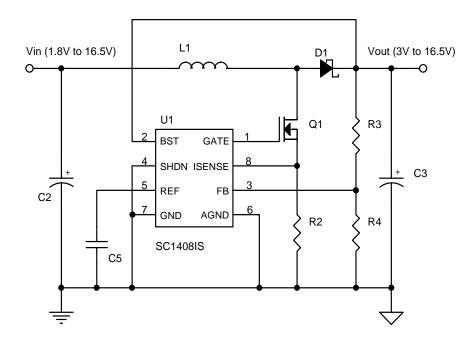
ORDERING INFORMATION

Part Number ⁽¹⁾	Package	Temp. Range (T _A)
SC1408IS.TR	SO-8	-40° to +85°C
SC1408IMS.TR	MSOP-8	

Note:

(1) Only available in tape and reel packaging. A reel contains 2500 devices.

TYPICAL APPLICATION - BOOST CONFIGURATION



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ABSOLUTE MAXIMUM RATINGS

Parameter	Symbol	Maximum	Units
Input Voltage	BST to GND	-0.3 to 18	V
Small Signal Ground to Power Ground	GND to AGND	±0.1	V
GATE to GND		-0.3 to VBST+0.3	V
FB, SHDN, REF, ISENSE to GND		-0.3 to min. of VBST+0.3 or 5	V
Operating Temperature	T _A	-40 to +85	°C
Junction Temperature Range	TJ	-40 to +150	°C
Storage Temperature	T _{STG}	-65 to +160	°C
Lead Temperature (Soldering) 10 seconds	TL	+300	°C
Thermal Resistance, Junction to Ambient SO-8 MSOP-8	θ _{JA}	165 206	°C/W
Thermal Resistance, Junction to Case SO-8/MSOP-8	θ_{JC}	40	°C/W

ELECTRICAL CHARACTERISTICS⁽¹⁾

Unless specified: $V_{OUT} = 5V$; $I_{LOAD} = 0mA$; $T_A = +25^{\circ}C$

PARAMETER	SYM	CONDITIONS		MIN	ТҮР	MAX	UNITS
Input Voltage		$T_A = 25^{\circ}C$		1.8		16.5	V
		$T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$		1.8		16.5	V
Supply Current		V _{OUT} = 16.5V, SHDN ≤ 0.4V	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$		110	140	uA
		$V_{OUT} = 10V,$ 1.6V \leq SHDN \leq 5V	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$		2	10	μA
Output Voltage		$V_{IN} = 2.0V$ to 5.0V,	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	4.800	5.0	5.200	V
Load Regulation		$V_{IN} = 2.0V, V_{OUT} = 5V, I_{LOAD} = 0mA \text{ to } 500mA$			60		mV/A
Line Regulation		$V_{IN} = 2.7V$ to 4.0V, $V_{OUT} = 5V$, $I_{LOAD} = 500$ mA			7		mV/V
Minimum Start Up Voltage		No load				1.8	V
Maximum Switch On Time	T _{ON}			9.6	16	22.4	μs
Minimum Switch Off Time	T _{OFF}			1.4	2.3	3.2	μs
Efficiency		$V_{IN} = 4V, V_{OUT} = 5V, I_{LOAD} = 500 \text{mA}$			87		%
Reference Voltage	V_{REF}	$I_{REF} = 0\mu A$	$T_A = -40^{\circ}C \text{ to } +85^{\circ}C$	1.176	1.200	1.224	V
Reference Load Regulation		0μA <u>≤</u> I _{REF} <u>≤</u> 100μA			-4	10	mV
Reference Line Regulation		$5V \le V_{OUT} \le 16.5V$			40	100	μV/V
FB Trip Point Voltage	V_{FB}	$T_{A} = 25^{\circ}C$ $T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$		1.176	1.200	1.224	V
FB Input Current	I _{FM}	$T_{A} = 25^{\circ}C$ $T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$			-4	<u>+</u> 40	nA



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ELECTRICAL CHARACTERISTICS⁽¹⁾

Unless specified: $V_{OUT} = 5V$; $I_{LOAD} = 0mA$; $T_A = +25^{\circ}C$

PARAMETER	SYM	CONDITIONS		MIN	ТҮР	MAX	UNITS
SHDN Input High Voltage	V _{IH}	V _{OUT} = 2.7V to 16.5V		1.6			V
SHDN Input Low Voltage	V _{IL}	V _{OUT} = 2.7V to 16.5V				0.4	V
SHDN Input Current	I _{IN}	$V_{OUT} = 16.5V$, SHDN = 0V or 5V				<u>+</u> 1	μA
Current Limit Trip Level	V _{cs}	$V_{OUT} = 3V \text{ to } 16.5V$	$T_{A} = 25^{\circ}C$ $T_{A} = -40^{\circ}C \text{ to } +85^{\circ}C$	85 80	100	115 120	mV
ISENSE Input Current	I _{SENSE}				0.01	<u>+</u> 1	μA
GATE Rise Time		$V_{OUT} = 5V$, 1nF from GATE to GND			50		ns
GATE Fall Time		$V_{OUT} = 5V$, 1nF from GATE to GND			50		
GATE On Resistance		GATE = high or low			15	30	Ω

NOTE:

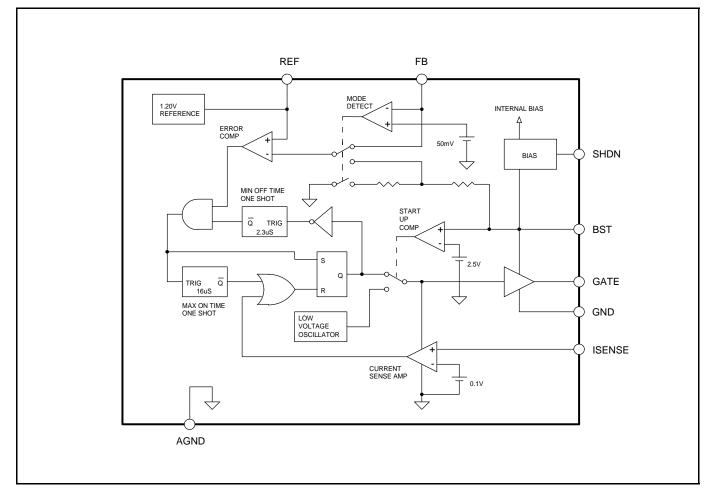
(1) This device is ESD sensitive. Use of standard ESD handling precautions is required.



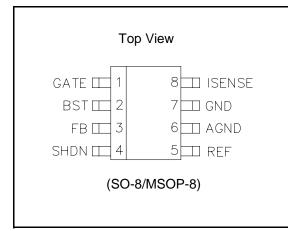
LOW VOLTAGE, BOOST DC-DC CONTROLLER

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BLOCK DIAGRAM



PIN CONFIGURATION



PIN DESCRIPTION

Pin #	Pin Name	Pin Function
1	GATE	Gate drive output.
2	BST	Supply voltage.
3	FB	Voltage feedback.
4	SHDN	Logic high shuts down the converter.
5	REF	Reference output pin.
6	AGND	Small signal analog and digital ground.
7	GND	Power ground.
8	ISENSE	Current sense pin.



Fig. 1: Typical Application - Boost Configuration

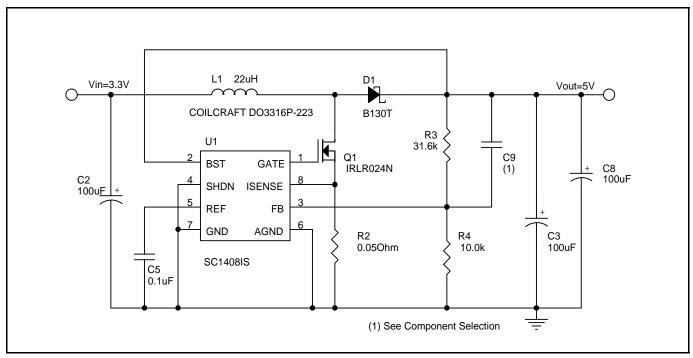


Fig. 2: Typical Application - Buck/Boost (SEPIC) Configuration

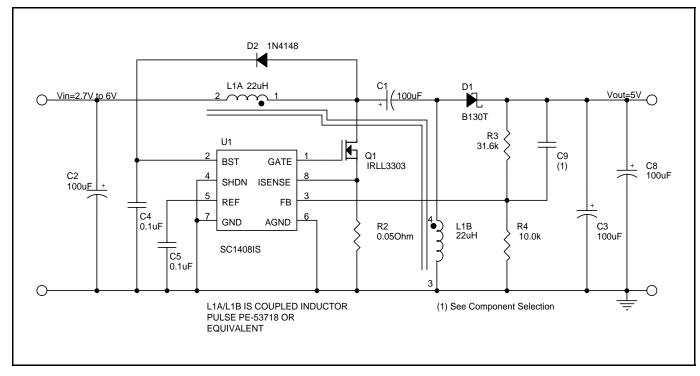




Fig. 3: Achieving output voltages greater than 16.5V

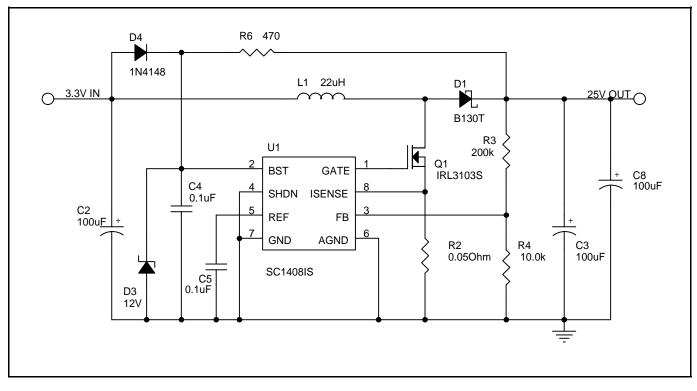
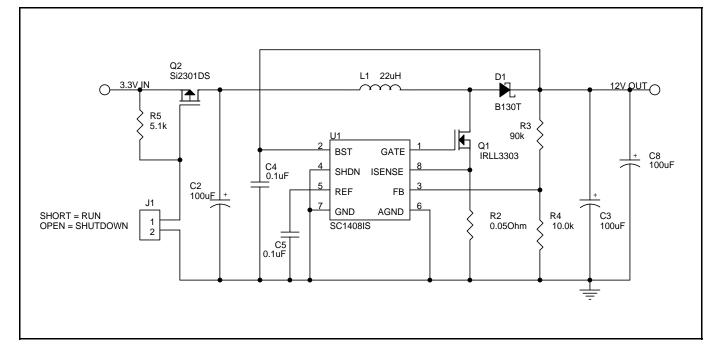


Fig. 4: Implementing shutdown with input/output isolation





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THEORY OF OPERATION

The SC1408 is a modified hysteretic boost converter controller. The power switch is turned on when the output voltage falls slightly below it's setpoint. It remains on for approximately 16us, or until the inductor current reaches limit, whichever occurs first. The power switch is then turned off for 2.3µs, or until the output voltage once again falls below setpoint, whichever occurs last.

The SC1408 is normally powered from the output voltage. Internal circuitry, such as the bandgap, comparators and one shots will not function properly until the BST pin voltage reaches 2.5V. To ensure startup at low input voltages, the normal control circuitry is disabled and a special, low voltage start up oscillator generates an approximate square wave at the GATE pin, initiating boost action. When the output voltage reaches 2.5V, the normal control circuitry is enabled and the start up oscillator shuts down.

To conserve power, a SHDN pin is provided which, when pulled high, shuts down most internal circuitry. The output voltage will then be one diode drop below the input.

COMPONENT SELECTION

Boost Converter

RSENSE

The value of the sense resistor is the primary determining factor for maximum output current. The SC1408 has a fixed current limit voltage threshold, which is developed by the peak inductor current flowing through RSENSE. RSENSE may be determined either from the maxi- Diode mum output current curves or from the equation below:

$$\begin{split} I_{O(MAX)} = & \frac{V_{CS}}{R_{SENSE}} \bigg(1 - \frac{V_O + V_F - V_{IN}}{V_O + V_F - V_{FET}} \bigg) \\ & - \frac{t_{off}}{2L} \bigg(\frac{(V_{IN} - V_{FET})(V_O + V_F - V_{IN})}{V_O + V_F - V_{FET}} \bigg) \end{split}$$

Where :

 V_{F} = Output Diode Forward Voltage Drop

V_{FET} = Voltage across FET, R_{SENSE} and Inductor DCR

In the equation above, the use of 2.3µs for t_{off} may lead to slightly optimistic current values for low V_0/V_{IN} ratios. The theoretical curves use the actual value of t_{off} , V_{F} =0.5V, V_{FET} =0.3V and V_{CS} =0.08V and are generated for L= 22μ H.

Output Voltage

Output voltage can be set to 5V by connecting the FB

pin to GND, or to any voltage in the 3.0V to 16.5V range using external divider resistors.

The bottom resistor in the divider chain (R4) should be $300k\Omega$ or less and the top resistor (R3 in the application circuits) can be calculated from:

$$3 = R4 \left(\frac{V_0}{V_{REF}} - 1 \right)$$

Inductor

R

The SC1408 will work with a wide range of inductor values. A good choice for most applications is 22µH. Smaller inductor values result in higher peak currents and increased output ripple, while larger values will result in slower loop response.

Transistor Selection

Normally the power switch will be an N-channel MOS-FET, although in certain circumstances an NPN bipolar may be substituted.

The choice of FET can be critical, especially in battery powered applications where the converter must be able to use all of the available energy in the battery. This requires that the converter be capable of starting up from very low input voltages. For example a two cell alkaline system's terminal voltage will drop to 1.8V as it approaches full discharge. For these demanding applications, a FET with low $V_{\mbox{\scriptsize GS(th)}}$ is required. A good rule of thumb is that $V_{GS(th)}$ should be at least 0.5V less than the minimum input voltage.

For most applications, a Schottky diode should be used as the output rectifier. It will be subjected to reverse voltages of at least V_o, and average current will be equal to the output current. Industry standard 1N5817 series or an equivalent surface mount part would be suitable.

Output Capacitors

Output capacitors should be low ESR to minimize ripple voltage and maximize efficiency. Low ESR tantalums, OSCONs or the newer Polymer capacitors should be used. Ripple voltage will be approximately:

$$V_{\text{RIPPLE}} = \frac{V_{\text{CS}} * R_{\text{ESR}}}{R_{\text{SENSE}}}$$

Input Capacitors

Input capacitors on a boost converter are less critical than the output capacitors, since there are no fast current pulses drawn from the input supply. A 100µF tantalum will be adequate for most applications.

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Feed Forward Capacitor

Although converters based on the SC1408 are stable, with no possibility of oscillation, they are susceptable to "mode switching" at intermediate current levels. This leads to increased ripple voltage and slightly reduced efficiency. Mode switching can be eliminated by a suitable choice of C9. It is possible to empirically select C9. Start with a value of about 100pF and adjust until all low frequency output ripple is eliminated at the desired output current.

See AN99-15 "SC1408 Operating Modes" for a full discussion of the origins of "Mode switching" and a more analytical approach to the selection of C9.

COMPONENT SELECTION

SEPIC Converter

RSENSE

Again, with the SEPIC topology, the value of the sense resistor is the primary determining factor for maximum output current. The simplest approach to select RSENSE is to add Vin to Vo and use this value as the output voltage in the output current curves or in the equation for Boost converter.

Output Voltage

Output voltage setting works exactly the same in SEPIC topology as in Boost, including the ability to set to 5V by connecting the FB pin to GND. Care must be taken to ensure that the IC supply (pin2; BST) does not exceed its 16.5V rating. In the circuit of Fig.2: This requires maximum output voltage to be limited to 16.5V-Vin. Higher output voltages are possible with different IC supply strategies.

Inductor

The SEPIC topology requires a coupled inductor. Again a good choice for most applications is 22uH. Smaller inductor values result in higher peak currents and increase output ripple, while larger values will result in slower loop response.

Transistor Selection

The choice of FET can be critical, especially in battery powered applications where the converter must be able to use all of the available energy in the battery. This requires that the converter be capable of starting up from very low input voltages. For example a two cell alkaline system's terminal voltage will drop to 1.8V as it approaches full discharge. For these demanding applications, a FET with low $V_{GS(th)}$ is required. A good rule of thumb is that $V_{GS(th)}$ should be at least 0.5V less than the minimum input voltage.

Diode

For most applications, a Schottky diode should be used as the output rectifier. It will be subjected to reverse voltages of at least $V_{\rm O}$ + $V_{\rm IN}$ and average current equal to the output current. Industry standard 1N5817 series or an equivalent surface mount part would be suitable.

Output Capacitors

Output capacitors should be low ESR to minimize ripple voltage and maximize efficiency. Low ESR tantalums, OSCONs or the newer Polymer capacitors should be used.

Input Capacitors

Input capacitors on a SEPIC converter are less critical than the output capacitors, since there are no fast current pulses drawn from the input supply. A 100μ F tantalum will be adequate for most applications.

Series Capacitors

The Series capacitor(s) must be capable of handling an RMS current given by:-

$$I_{\text{RMS}} = I_{\text{O}} \sqrt{\frac{V_{\text{O}} + 0.5}{V_{\text{IN}}}}$$

Feed Forward Capacitor

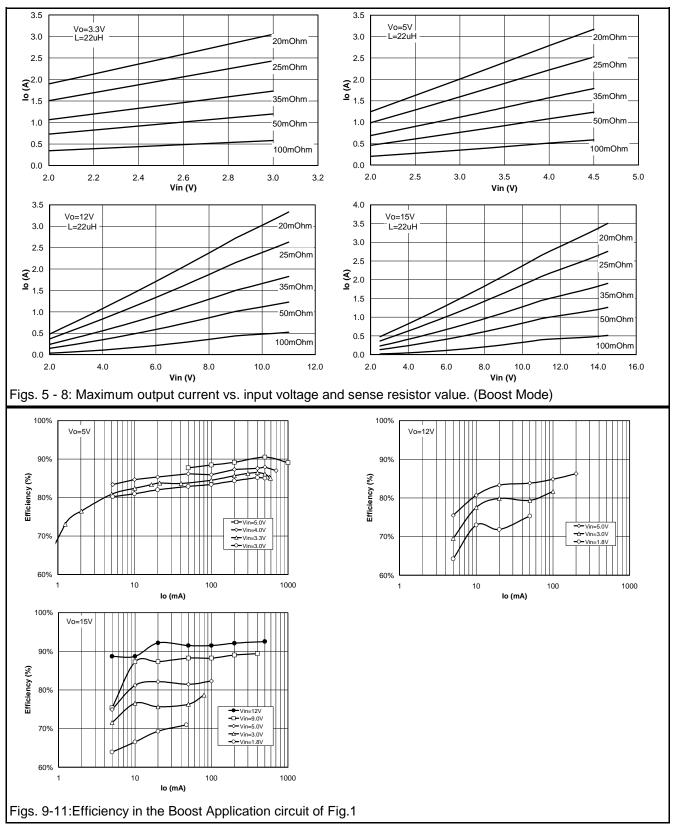
The feed forward capacitor should be selected in the same way as for a Boost application.

LAYOUT GUIDELINES

The SC1408 is fairly insensitive to layout, however following some simple guidelines will help ensure successful implementation.

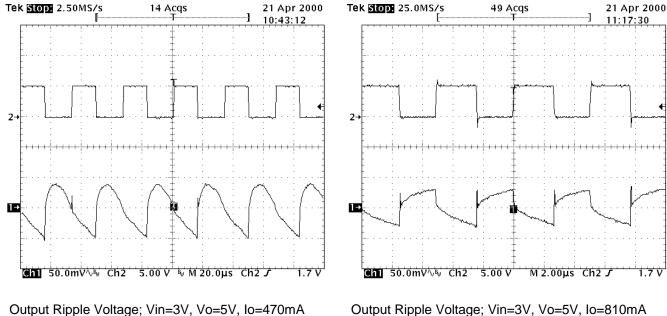
Whenever possible, lay the circuitry out over a ground plane. Connect AGND and GND together at the IC and return to the ground plane with one or two vias. Place the current sense resistor (R2), the REF decoupling capacitor (C5) and the divider resistors (R3 and R4) close to the IC, Return the ground side of these components to the ground plane close to the AGND/GND pin vias. Connect the top side of the sense resistor to ISENSE with a short trace and the source of Q1 directly to the sense resistor. Make the output loop Q1, D1 and the output capacitors (C3, C8) as small as possible to minimize EMI.





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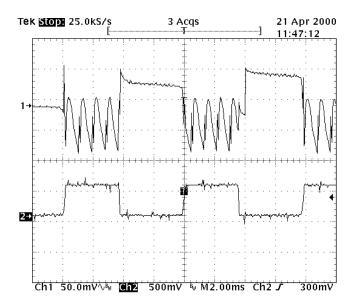




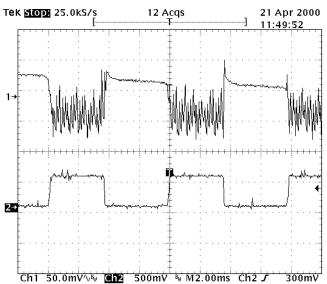
Ch1 = Output Ripple

Ch2 = Voltage at GATE pin

Output Ripple Voltage; Vin=3V, Vo=5V, Io=810mA Ch1 = Output Ripple Ch2 = Voltage at GATE pin



Load Transient; Vin=3V, Vo=5V, Io=0 to 500mA Ch1 = Output Voltage Ch2 = Load Current (0.5A/div)



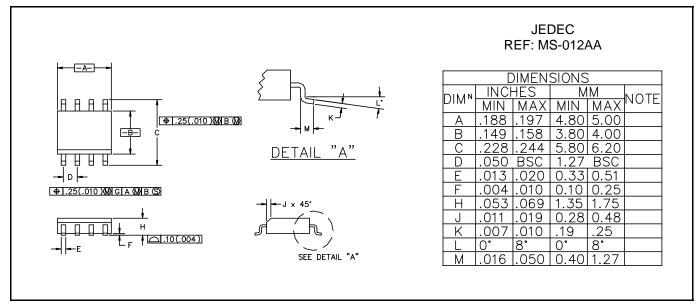
Load Transient; Vin=2V, Vo=5V, Io=0 to 500mA Ch1 = Output Voltage Ch2 = Load Current (0.5A/div)



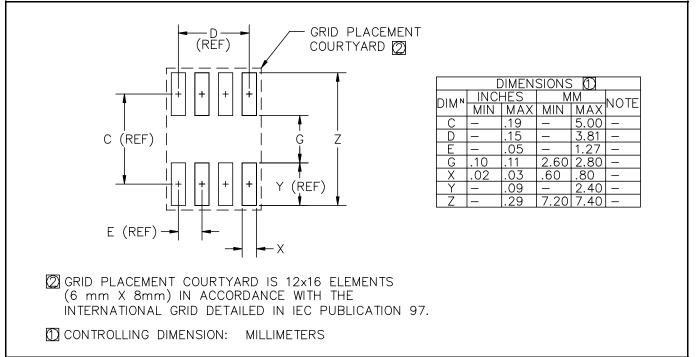
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OUTLINE DRAWING - SO-8

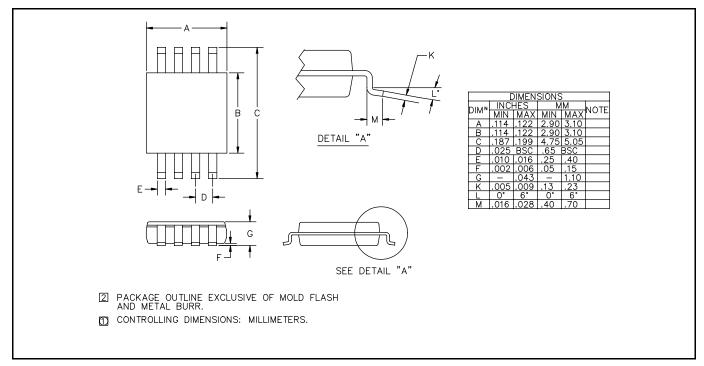


LAND PATTERN - SO-8

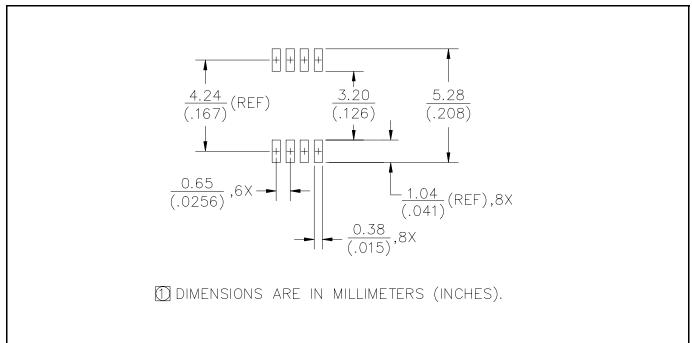




OUTLINE DRAWING - MSOP-8



LAND PATTERN - MSOP-8



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