

General Description

The SPT207 is a wideband, low distortion operational amplifier designed specifically for applications requiring both high speed and wide dynamic range. Utilizing a proprietary current feedback architecture, the SPT207 offers performance far superior to that of conventional voltage feedback op amps.

The most attractive feature of the SPT207 is its extremely low distortion: -80/-85dBc 2nd/3rd harmonics at 20MHz ($2V_{pp}$, $R_L = 200\Omega$). The SPT207 also provides -3dB bandwidth of 170MHz at a gain of +20, settles to 0.1% in 22ns and slews at a rate of 2400V/ μ s, yet is unity-gain stable without external compensation. The combination of these features positions the SPT207 as the right choice for high speed applications requiring exceptional signal purity.

High speed, high resolution A/D and D/A converter systems requiring low distortion operation will find the SPT207 an excellent choice. Wide dynamic range systems such as radar and communication receivers will find that the SPT207's low harmonic distortion and low noise make it an attractive high speed solution.

The addition of the SPT207 to the 205/206 Series of high speed operational amplifiers broadens the selection of features available from which to choose. The SPT205 offers low power operation, the SPT206 offers higher drive operation, and the SPT207 offers operation with extremely low distortion, all of which are pin compatible and overdrive protected.

The SPT207 is constructed using thin film resistor/bipolar transistor technology, and is available in the following versions:

- SPT207AIH -25°C to +85°C 12-pin TO-8 can
- SPT207AMH -55°C to +125°C 12-pin TO-8 can, features burn-in and hermetic testing

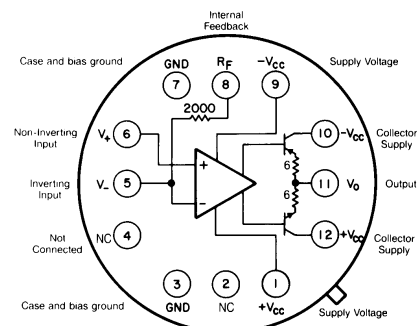
Features

- -3dB bandwidth of 180MHz
- 70MHz large signal bandwidth ($20V_{pp}$)
- 0.1% settling in 19ns
- Overdrive protected
- Output may be current limited
- Stable without compensation
- $3M\Omega$ input impedance

Applications

- Fast, precision A/D conversion
- Automatic test equipment
- Input/output amplifiers
- Photodiode, CCD preamps
- High-speed modems, radios
- Line drivers

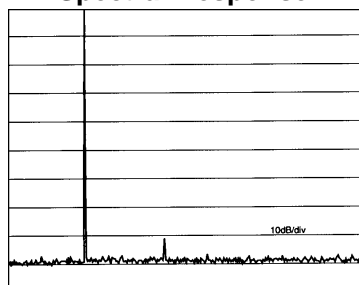
Bottom View



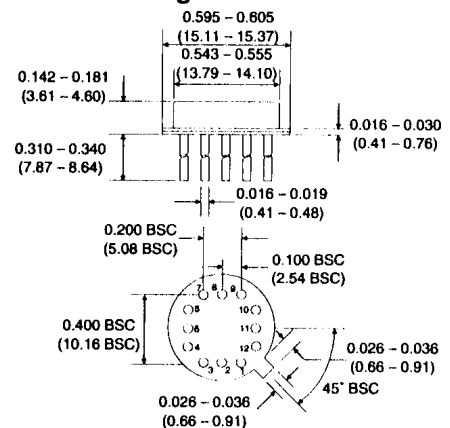
Typical Performance

parameter	gain setting						units
	+7	+20	+50	-1	-20	-50	
-3dB bandwidth	220	170	80	220	130	80	MHz
rise time	1.7	2.2	4.7	1.7	2.9	4.7	ns
slew rate	2.4	2.4	2.4	2.4	2.4	2.4	V/ns
settling time (to 0.1%)	22	22	20	21	20	19	ns

Spectral Response



Package Dimensions



SPT207 Electrical Characteristics ($V_A = +20V, V_{CC} = \pm 15V, R_L = 200\Omega, R_f = 2k\Omega$; unless specified)

PARAMETERS	CONDITIONS	TYP	MAX & MIN RATINGS				UNITS	SYMBOL
Ambient Temperature	SPT207AIH	+25°C	-25°C	+25°C	+85°C			
Ambient Temperature	SPT207AMH	+25°C	-55°C	+25°C	+125°C			
FREQUENCY DOMAIN RESPONSE								
† -3dB bandwidth	$V_{out} < 2V_{pp}$	170	>140	>140	>125	MHz	SSBW	
	$V_{out} < 10V_{pp}$	100	>72	>80	>80	MHz	LSBW	
gain flatness	$V_{out} < 2V_{pp}$							
† peaking	0.1 to 35MHz	0	<0.3	<0.3	<0.5	dB	GFPL	
† peaking	>35MHz	0	<0.5	<0.5	<0.8	dB	GFPH	
† rolloff	at 70MHz	—	<0.8	<0.8	<0.8	dB	GFR	
group delay	to 70MHz	$3.0 \pm .2$	—	—	—	ns	GD	
linear phase deviation	to 50MHz	0.8	<3.0	<2.0	<3.0	°	LPD	
TIME DOMAIN RESPONSE								
rise and fall time	2V step	2.2	<2.6	<2.6	<3.0	ns	TRS	
	10V step	4.8	<5.5	<5.5	<5.5	ns	TRL	
settling time to 0.1%	10V step, note 2	22	<27	<27	<27	ns	TS	
to 0.05%	10V step, note 2	24	<30	<30	<30	ns	TSP	
overshoot	5V step	7	<14	<14	<14	%	OS	
slew rate	$20V_{pp}$ @ 50MHz	2400	>1800	>2000	>2000	V/ μ s	SR	
DISTORTION AND NOISE RESPONSE, note 3								
†2nd harmonic distortion	$2V_{pp}$, 20MHz, $R_L = 200\Omega$	-80	<-68	<-76	<-76	dBc	HD2	
	$R_L = 100\Omega$	-69	<-64	<-64	<-64	dBc	HD2	
†3rd harmonic distortion	$2V_{pp}$, 20MHz, $R_L = 200\Omega$	-85	<-76	<-76	<-76	dBc	HD3	
	$R_L = 100\Omega$	-69	<-64	<-64	<-64	dBc	HD3	
equivalent noise input voltage	>100kHz	1.6	<1.8	<1.8	<1.8	nV/ \sqrt{Hz}	VN	
inverting current	>100kHz	20	<23	<23	<23	pA/ \sqrt{Hz}	ICN	
non-inverting current	>100kHz	2.2	<2.5	<2.5	<2.5	pA/ \sqrt{Hz}	NCN	
noise floor	>100kHz	-158	<-157	<-157	<-157	dBm _{1Hz}	SNF	
integrated noise	1kHz to 150MHz	33	<38	<38	<38	μ V	INV	
integrated noise	5MHz to 150MHz	33	<38	<38	<38	μ V	INV	
STATIC DC PERFORMANCE								
*input offset voltage		3.5	<8.0	<8.0	<11.0	mV	VIO	
average temperature coefficient		11	<25	<25	<25	μ V/°C	DVIO	
*input bias current	non-inverting	3.0	<25	<15	<15	μ A	IBN	
average temperature coefficient		15	<100	<100	<100	nA/°C	DIBN	
*input bias current	inverting	2.0	<22	<10	<25	μ A	IBI	
average temperature coefficient		20	<150	<150	<150	nA/°C	DIBI	
*power supply rejection ratio		69	>55	>55	>55	dB	PSRR	
common mode rejection ratio		60	>50	>50	>50	dB	CMRR	
*supply current	no load	25	<27	<27	<29	mA	ICC	
MISCELLANEOUS PERFORMANCE								
non-inverting input resistance	DC	3.0	>1.0	>1.0	>1.0	M Ω	RIN	
non-inverting input capacitance	70MHz	5.0	<7.0	<7.0	<7.0	pF	CIN	
output impedance	DC	—	<0.1	<0.1	<0.1	Ω	RO	
output voltage range	no load	± 12	> ± 11	> ± 11	> ± 11	V	VO	
internal feedback resistor		2.0	—	—	—	k Ω	RF	
absolute tolerance		—	—	<0.2	—	%	RFA	
temperature coefficient		—	—	-100 \pm 40	—	ppm/°C	RFTC	
inverting input current self limit		2.2	<3.0	<3.0	<3.2	mA	ICL	

Min/max ratings are based on product characterization and simulation. Individual parameters are tested as noted. Outgoing quality levels are determined from tested parameters.

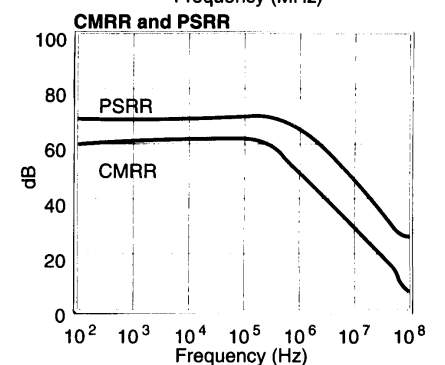
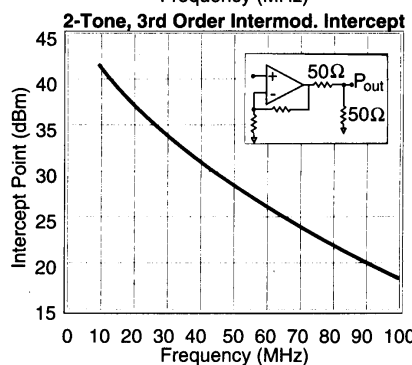
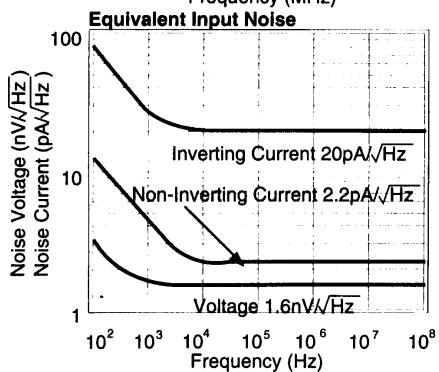
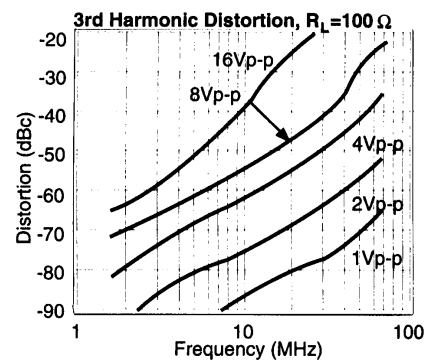
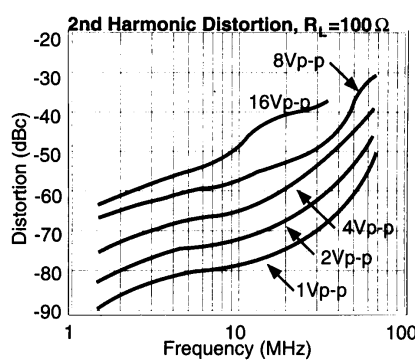
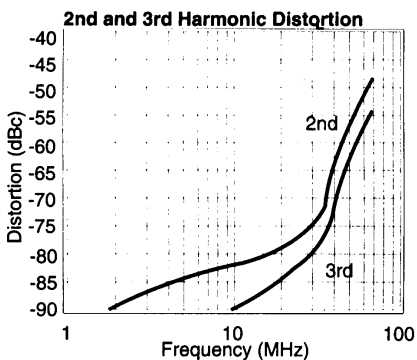
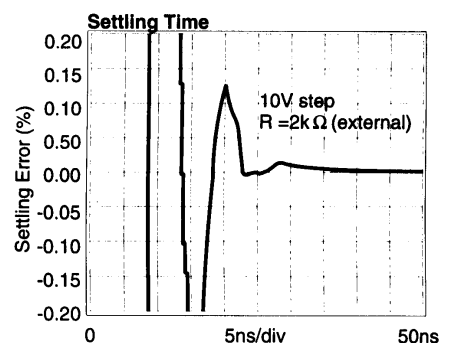
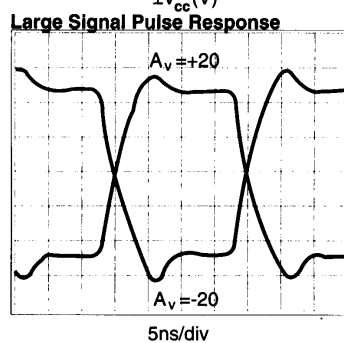
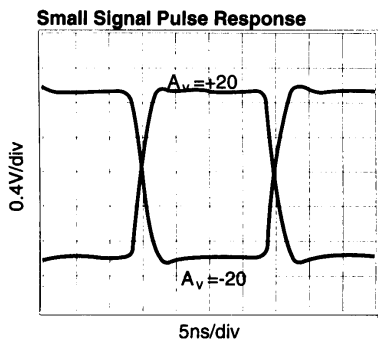
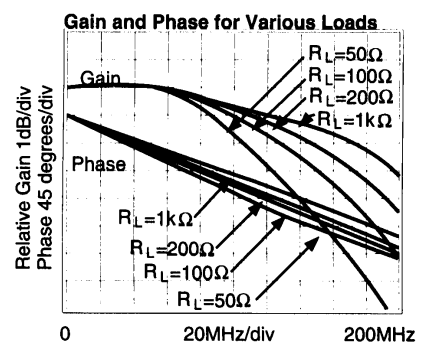
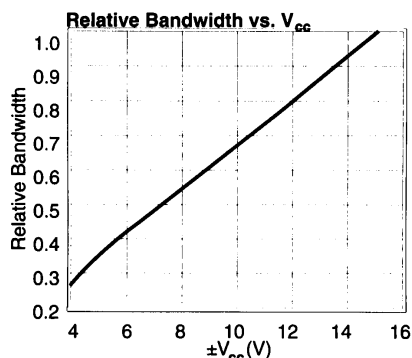
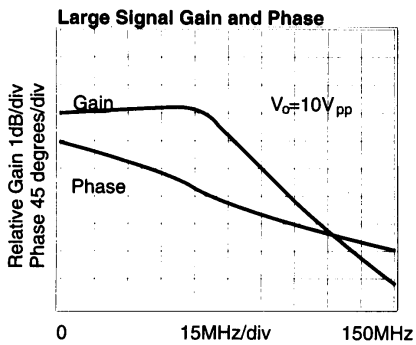
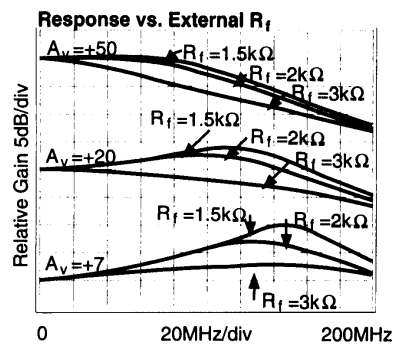
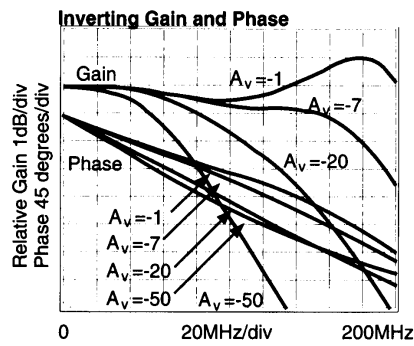
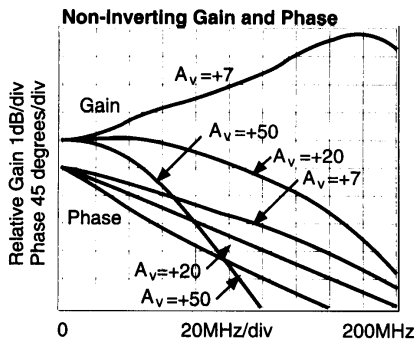
Absolute Maximum Ratings

V_{CC}	$\pm 20V$
I_{out}	$\pm 150mA$
V_{CM}, V_{out}	$V_{CC} > 15V$ $\pm (29 - V_{CC})V$
	$V_{CC} \leq 15V$ $\pm (V_{CC} - 1)V$
differential input voltage	$\pm 3V$
junction temperature	+175°C
operating temperature range	AIH: -25°C to +85°C
	AMH: -55°C to +125°C
storage temperature	-65°C to +150°C
lead temperature (soldering 10s)	+300°C

Recommended Operating Conditions

V_{CC}	$\pm 5V$ to $\pm 15V$
I_{out}	$\pm 100mA$
V_{CM}	$\pm (V_{CC} - 5)V$
gain range	+7 to +50, -1 to -50
note 1: * AIH, AMH	100% tested at 25°C.
† AIH	100% tested at +25°C and sample tested at -55°C and +125°C.
† AMH	sample tested at +25°C.
note 2:	Settling time specifications require the use of an external feedback resistor (2k Ω).
note 3:	AIH and AMH units tested with $R_L = 200\Omega$.

SPT207 Typical Performance Characteristics ($T_A = +25^\circ$, $A_V = +20$, $V_{CC} = \pm 15V$, $R_L = 200\Omega$; unless specified)



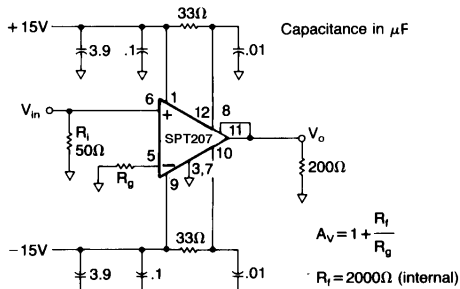


Figure 1: recommended non-inverting gain circuit

Overdrive Protection

Unlike most other high-speed op amps, the SPT207 is not damaged by saturation caused by overdriving input signals (where $V_{in} \times \text{gain} > \text{max. } V_{out}$). The SPT207 self limits the current at the inverting input when the output is saturated (see the inverting input current self limit specification); this ensures that the amplifier will not be damaged due to excessive internal currents during overdrive. For protection against input signals which would exceed either the maximum differential or common mode input voltage, the diode clamp circuits below may be used.

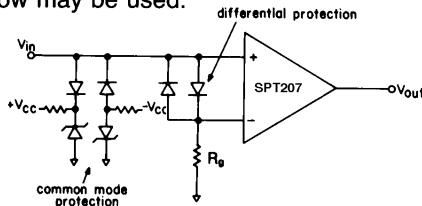


Figure 3: diode clamp circuits for common mode and differential mode protection

Short Circuit Protection

Damage caused by short circuits at the output may be prevented by limiting the output current to safe levels. The most simple current limit circuit calls for placing resistors between the output stage collector supplies and the output stage collectors (pins 12 and 10). The value of this resistor is determined by:

$$R_c = V_c / I_l - R_l$$

Where I_l is the desired limit current and R_l is the minimum expected load resistance (0Ω for a short to ground). Bypass capacitors of $0.01\mu\text{F}$ on should be used on the collectors as in Figures 1 and 2.

A more sophisticated current limit circuit which provides a limit current independent of R_l is shown below.

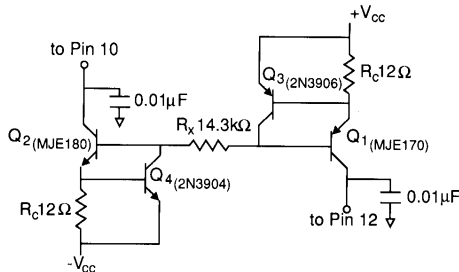


Figure 4: active current limit circuit (50mA)

With the component values indicated, current limiting occurs at 50mA. For other values of current limit (I_l), select R_c to equal V_{be}/I_l . Where V_{be} is the base to emitter voltage drop of Q3 (or Q4) at a current of $[2V_{cc} - 1.4]/R_x$, where $R_x \leq [(2V_{cc} - 1.4)/I_l] B_{min}$. Also, B_{min} is the minimum beta of Q1 (or Q2) at a current of I_l . Since the limit current depends on V_{be} , which is temperature dependent, the limit current is likewise temperature dependent.

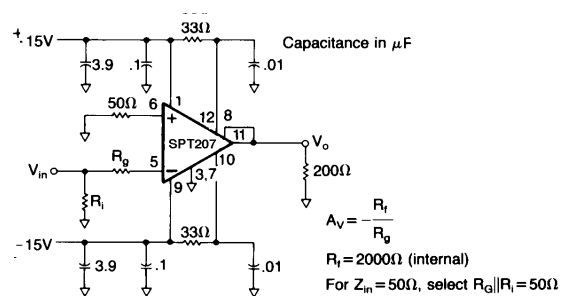


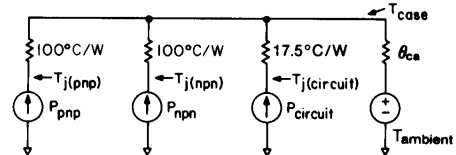
Figure 2: recommended inverting gain circuit

Controlling Bandwidth and Passband Response

In most applications, a feedback resistor value of $2k\Omega$ will provide optimum performance; nonetheless, some applications may require a resistor of some other value. The response versus R_f plot on the previous page shows how decreasing R_f will increase bandwidth (and frequency response peaking, which may lead to instability). Conversely, large values of feedback resistance tend to roll off the response.

The best settling time performance requires the use of an external feedback resistor. (Use of the internal resistor results in 0.1% to 0.2% settling tail.) The settling performance may be improved slightly by adding a capacitance of 0.4pF in parallel with the feedback resistor. (Settling time specifications reflect performance with an external feedback resistor but with no external capacitance.)

Thermal Model



$$P_{circuit} = [(+V_{cc}) - (-V_{cc})]^2 / 1.77k\Omega$$

$$P_{xxx} = [(\pm V_{cc}) - V_{out} - (I_{col}) (R_{col} + 6)] (I_{col})$$

(% duty cycle)

(For positive V_o and V_{cc} , this is the power in the npn output stage.)
 (For negative V_o and V_{cc} , this is the power in the pnp output stage.)

- $\theta_{ca} = 65^\circ\text{C/W}$ in still air without a heatsink
- 35°C/W in still air with a Thermalloy 2268B
- 15°C/W in 300ft/min air with a Thermalloy 2268B (Thermalloy 2240 works equally well.)

$I_{col} = V_{out}/R_{load}$ or 3mA, whichever is greater. (Include feedback R in R_{load} .)

R_{col} is a resistor (33Ω recommended) between the xxx collector and $\pm V_{cc}$.

$$T_j(pnp) = P_{pnp}(200 + \theta_{ca}) + (P_{cir} + P_{nnp}) \theta_{ca} + T_a$$

similar for $T_j(npn)$.

$$T_j(cir) = P_{cir}(17.5 + \theta_{ca}) + (P_{pnp} + P_{nnp}) \theta_{ca} + T_a$$

Printed Circuit Layout

As with any high frequency device, a good PCB layout will enhance the performance of the SPT207. Good ground plane construction and power supply bypassing close to the package are critical to achieving full performance. In the non-inverting configuration, the amplifier is sensitive to stray capacitance to ground at the inverting input. Hence, the inverting node connections should be small with minimal stray capacitance to the ground plane or other nodes. Shunt capacitance across the feedback resistor should not be used to compensate for this effect.

Evaluation PC boards (inverting and non-inverting) for the SPT207 are available.

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